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RESEARCH MEMORANDUM

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for the

U. S. Air Force

INVESTIGATION OF A 1/4-SCALE MODEL OF THE REPUBLIC F-105
AIRPLANE IN THE Langley 19-FOOT PRESSURE TUNNEL

INFLUENCE OF TRAILING-EDGE FLAP SPAN AND DEFLECTION
ON THE LONGITUDINAL CHARACTERISTICS

By Patrick A. Cancro and H. Neale Kelly

Langley Aeronautical Laboratory
Langley Field, Va.

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INFLUENCE OF TRAILING-EDGE FLAP SPAN AND DEFLECTION

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SUMMARY

Development tests on a 1/4-scale model of the Republic F-105 airplane are being conducted in the Langley 19-foot pressure tunnel. The second phase, the results of which are presented herein, was made at a Reynolds number of 9.0×10^6 and a Mach number of 0.20. Exploratory tests were made at Reynolds numbers of 3, 6, 7, and 8×10^6 and corresponding Mach numbers of 0.06, 0.13, 0.16, and 0.18.

The purpose of the present tests was to obtain the longitudinal force and moment characteristics of the model equipped with trailing-edge flaps of various spans and deflections. In addition, an investigation was made to show the effect of Reynolds number and also the effect of a transonic inlet with the original horizontal tail and with a larger span horizontal tail.

In order to expedite the issuance of the data for this airplane, no analysis of the data has been presented.

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INTRODUCTION

The F-105 airplane is a 45° sweptback, midwing, low-tail, supersonic fighter-bomber being developed by the Republic Aviation Corporation for the U. S. Air Force. At the request of the Air Force, development tests on a $1/4$ -scale model of the F-105 are being conducted in the Langley 19-foot pressure tunnel to determine the low-speed aerodynamic characteristics of the basic design and, if necessary, to develop modifications which will provide the model with satisfactory low-speed stability and control characteristics.

The initial longitudinal stability and control tests of a model of the F-105 airplane (ref. 1) indicated that the model possessed acceptable longitudinal stability characteristics as long as the trailing-edge flaps were neutral. With the trailing-edge flaps deflected, however, it was found that the model did not possess sufficient static margin at the most rearward anticipated center-of-gravity position (38 percent mean aerodynamic chord). Furthermore, because of the nonlinear lift characteristics of the horizontal tail and the associated pitch-up, satisfactory stability could not be obtained at the most forward center-of-gravity position (22 percent mean aerodynamic chord). Although various other modifications were attempted (see ref. 1), satisfactory stability could only be obtained by reducing either the flap span or deflection, or both.

The primary purpose of the tests presented herein was to determine the greatest flap span and deflection that could be used and still retain an adequate static margin up to and including the landing angle of attack. These tests were made at tail incidences required to trim the model at an angle of attack of 12° for the 22-percent and 38-percent center-of-gravity locations. In addition, tests were made at various Reynolds numbers and with a transonic-type elliptical inlet and larger span horizontal tail. The model was tested through an angle-of-attack range of -4° through the stall.

COEFFICIENTS AND SYMBOLS

C_L lift coefficient, Lift/qS

$C_{L_{max}}$ maximum lift coefficient

C_D drag coefficient, Drag/qS

C_m pitching-moment coefficient, Pitching moment/qSc
(an additional subscript denotes location of center of gravity)

- b wing span, ft
- c local streamwise chord, ft
- \bar{c} mean aerodynamic chord, $\frac{2}{S} \int_0^{b/2} c^2 dy$, ft
- y spanwise distance from plane of symmetry, ft
- z vertical distance from mean aerodynamic chord extended, ft
- α angle of attack, deg
- δ_f trailing-edge flap deflection, trailing edge down for positive deflection, deg
- δ_n drooped leading-edge flap deflection, leading edge down for positive deflection, deg
- i_t tail incidence relative to the wing-chord plane, trailing edge down for positive incidence, deg

MODEL

Model Description

The model was primarily of steel-reinforced wood construction; however, the inlets, trailing-edge flaps, and leading-edge flaps were aluminum.

Basic model.- The basic model for the longitudinal stability and control tests was a 1/4-scale model of the F-105 airplane wing, fuselage, and vertical tail. Principal dimensions and design features of the model and a photograph of the model installed in the Langley 19-foot pressure tunnel are presented in table I and figures 1 and 2.

It should be noted here that between the tests reported in reference 1 and the tests presented herein, the model was sent back to Republic Aviation Corporation for the fitting of additional control-setting brackets and a revision to the lateral-control system. In the course of these modifications, the wing contour and flap positioning were rechecked. The flap gap was found to be unsymmetrical and the wing leading-edge radius was not in agreement with the specified airfoil section ordinates. In consequence, the trailing-edge flap positioning was altered slightly

and the forward 10 percent of the wing was reworked to bring it into agreement with the calculated airfoil ordinates to within ± 0.003 inch.

Horizontal tail.- The horizontal tail was located at a tail height of $0.123b/2$ below the mean-aerodynamic-chord plane extended, and it was possible to obtain tail-incidence settings of 7° , 3.5° , 0° , -3.5° , -9.5° , -14° , -20° , and -25° . A larger span horizontal tail was also tested. Details of the horizontal tails may be seen in figure 1 and table I.

Trailing-edge flaps.- The wing was equipped with a single slotted trailing-edge flap which extended from $0.133b/2$ to $0.800b/2$. The flap was cut so that flaps extending from $0.133b/2$ to $0.600b/2$, $0.650b/2$, and $0.700b/2$ could also be tested. Hereinafter, the flap span is designated by the outboard end location in percent span. For example, the $0.133b/2$ to $0.600b/2$ span flap is identified as a 60-percent-span trailing-edge flap. The flap could be set at angles of 0° , 40° , and 46° perpendicular to the flap hinge line through the use of interchangeable steel positioning brackets. Details of the measured flap settings and gaps are compared with the design loft data furnished by Republic Aviation Corporation and may be seen in figure 3.

Leading-edge flaps.- An inversely tapered drooped leading-edge flap with interchangeable deflection brackets of 0° , 7.5° , 20° , and 30° perpendicular to the hinge line was provided as a stall-control device. Details of the leading-edge flap may be seen in figure 3 and table I.

External stores.- Except for a few tests, external stores representative of 450-gallon pylon-mounted fuel tanks were attached at the $0.606b/2$ station. Details of the external stores can be found in figure 4 and table I.

Inlets.- The model was equipped with either a supersonic-type or a transonic-type elliptical wing-root inlet. Photographs of these inlets may be seen in figure 5.

Model Nomenclature

Listed below are the designations given to the various component parts of the model. The complete model configurations are obtained by combining the appropriate model components with the basic model.

- A basic model (wing plus fuselage)
- E external stores
 - subscript: 0 indicates outboard location ($0.606b/2$)
 - suffix: 450 indicates 450-gallon fuel tank

- F single slotted trailing-edge flap
prefix: flap span (fraction of wing semispan)
subscript: deflection, trailing edge down for positive deflection, deg
- I wing-root inlet
subscript: SE indicates supersonic-type elliptical inlet
TE indicates transonic-type elliptical inlet
- N inversely tapered drooped leading-edge flap
subscript: deflection, leading edge down for positive deflection, deg
- T horizontal tail
prefix: vertical position (fraction of wing semispan)
subscript: incidence, trailing edge down for positive incidence, deg
superscript: * indicates increased tail span
- V vertical tail

TESTS

All tests reported herein were conducted in the Langley 19-foot pressure tunnel at a tunnel pressure of approximately $2\frac{1}{3}$ atmospheres.

For most of the tests, the Reynolds number, based on the mean aerodynamic chord, was 9.0×10^6 and the Mach number was 0.20. However, exploratory tests were made to determine the effect of Reynolds number. These tests were conducted at Reynolds numbers of 3.0, 6.0, 7.0, and 8.0×10^6 with corresponding Mach numbers of 0.06, 0.13, 0.16, and 0.18. The model was mounted on the normal three-support system at 0° angle of yaw and was tested through an angle-of-attack range of -4° through the stall.

Longitudinal characteristics of the model for the various flap span arrangements at a tail incidence required to trim this model at $\alpha = 12^\circ$ for the $0.22c$ and $0.38c$ center-of-gravity positions were obtained. A transonic-type elliptical inlet was tested and data were obtained with the original horizontal tail and with an increased span horizontal tail.

CORRECTIONS

Jet-boundary corrections determined by the method of reference 2 have been applied to all force and moment data. Corrections for support

tare and interference effects and for air-flow misalignment have not been applied. Internal drag of the inlets and duct system is included in the drag data presented herein.

PRESENTATION OF DATA

The comparison (fig. 6) of the results of tests for the flaps-neutral condition presented herein with tests of a comparable configuration presented in reference 1 shows the two sets of results to be similar except for small differences at the higher angles of attack. This indicates that the reworking of the wing leading edge that occurred between the initial and present tests had little effect on the measured characteristics.

Similar comparisons (fig. 7) with $\delta_f = 46^\circ$ show noticeable stability changes at a lift coefficient of about 0.8 between the initial tests (ref. 1) and the tests presented herein. The differences in test results shown in figure 7 are attributed to the change in flap positioning that occurred between the initial and present tests. This effect should be kept in mind in comparing the flap-deflected results presented herein with those presented in reference 1.

The longitudinal stability characteristics about the $0.25\bar{c}$ are summarized in tables II, III, and IV. The results of the tests about the $0.22\bar{c}$ and $0.38\bar{c}$ for the various flap configurations are contained in figures 8 to 21. A static-margin summary chart is presented in figure 22. The effect of various trailing-edge flap spans and the effect of various leading-edge flap deflections on the longitudinal stability characteristics may be seen in figures 23 and 24, respectively. Tests were made to determine the effect of Reynolds number on the longitudinal characteristics of the model, and the results are presented in figures 25 and 26. The data obtained with the transonic elliptical inlet can be found in figures 27 to 29. The results of a horizontal-tail span increase with the transonic elliptical inlet are presented in figure 30.

Langley Aeronautical Laboratory,

National Advisory Committee for Aeronautics,
Langley Field, Va., August 12, 1954.

Patrick A. Cancro
Patrick A. Cancro
Mechanical Engineer

Approved:

Eugene C. Draley

Eugene C. Draley
Chief of Full-Scale Research Division

H. Neale Kelly

H. Neale Kelly
Aeronautical Research Scientist

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REFERENCES

1. Kelly, H. Neale, and Cancro, Patrick A.: Investigation of a 1/4-Scale Model of the Republic F-105 Airplane in the Langley 19-Foot Pressure Tunnel - Longitudinal Stability and Control of the Model Equipped With a Supersonic-Type Elliptical Wing-Root Inlet. NACA RM SL54F28, U. S. Air Force, 1954.
2. Sivells, James C., and Salmi, Rachel M.: Jet-Boundary Corrections for Complete and Semispan Swept Wings in Closed Circular Wind Tunnels. NACA TN 2454, 1951.

TABLE I-- DESIGN CHARACTERISTICS OF THE REPUBLIC F-105 AIRPLANE AND THE 1/4-SCALE MODEL OF THE F-105 AIRPLANE

	Full-scale	1/4-scale
<u>Wing Assembly</u>		
Basic data:		
Root airfoil, measured parallel to airplane center line at $0.38b/2$	NACA 65A005.5	NACA 65A005.5
Tip airfoil, measured parallel to airplane center line	NACA 65A003.7	NACA 65A003.7
Angle of incidence, deg	0	0
Geometric twist, deg	0	0
Sweep of quarter-chord line (true), deg	45	45
Taper ratio	0.467	0.467
Aspect ratio (excluding inlet area)	3.182	3.182
Dihedral, deg	-3.5	-3.5
Dimensions:		
Root chord (theoretical), parallel to airplane center line, ft	15.000	3.750
Tip chord (theoretical), parallel to airplane center line, ft	7.000	1.750
Mean aerodynamic chord, parallel to airplane center line, ft	11.485	2.871
Location of mean aerodynamic chord, spanwise (projected), ft	7.690	1.933
Span, measured normal to airplane center line, ft	34.934	8.734
Area:		
Wing area (excluding inlet area), sq ft	385.0	24.062
<u>Horizontal-Tail Assembly</u>		
Basic data:		
Root airfoil, streamwise	NACA 65A006	NACA 65A006
Tip airfoil, streamwise	NACA 65A004	NACA 65A004
Taper ratio:		
Basic horizontal tail	0.456	0.456
Modified horizontal tail	0.401	0.401
Aspect ratio:		
Basic horizontal tail	3.06	3.06
Modified horizontal tail	3.49	3.49
Dihedral, deg	0	0
Dimensions:		
Root chord (theoretical), ft	7.50	1.875
Tip chord (theoretical):		
Basic horizontal tail, ft	3.42	0.855
Modified horizontal tail, ft	3.01	0.752
Mean aerodynamic chord (theoretical):		
Basic horizontal tail, ft	5.71	1.428
Modified horizontal tail, ft	5.58	1.395
Span:		
Basic horizontal tail, ft	16.67	4.168
Modified horizontal tail, ft	18.33	4.582
0.25 δ of wing to 0.25 δ of horizontal tail (theoretical):		
Basic horizontal tail, ft	20.68	5.232
Modified horizontal tail, ft	20.96	5.302
Vertical location below fuselage center line, in.	-18.00	-4.5

TABLE I.- DESIGN CHARACTERISTICS OF THE REPUBLIC F-105 AIRPLANE AND THE 1/4-SCALE MODEL OF THE F-105 AIRPLANE - CONTINUED

	Full-scale	1/4-scale
<u>Horizontal-Tail Assembly - Concluded</u>		
Area:		
Horizontal-tail area (theoretical):		
Basic, sq ft	90.97	5.685
Modified, sq ft	96.32	6.020
Horizontal-tail area (exposed):		
Basic, sq ft	60.77	3.798
Modified, sq ft	66.13	4.133
<u>Vertical-Tail Assembly</u>		
Basic data:		
Root airfoil, measured parallel to airplane center line at $0.167b/2$	NACA 65A006	NACA 65A006
Tip airfoil, measured parallel to airplane center line	NACA 65A004	NACA 65A004
Sweepback of quarter-chord line, deg	45	45
Aspect ratio (theoretical)	1.593	1.593
Taper ratio (theoretical)	0.365	0.365
Sweepback of rudder hinge line, deg	29.358	29.358
Rudder deflections, measured in a plane normal to the hinge line, deg	32 to -32	0,12,24,35
Dimensions:		
Root chord (theoretical), ft	10.03	2.508
Tip chord (theoretical), ft	3.67	0.9175
Mean aerodynamic chord (theoretical), ft	7.34	1.835
0.25c of wing to 0.25c of vertical tail (theoretical), ft	17.40	4.412
Vertical-tail height, measured from fuselage center line, ft	10.92	2.729
Rudder chord (average), ft	1.86	0.458
Rudder span, measured normal to fuselage center line, ft	6.83	1.708
Area:		
Vertical-tail area (theoretical), sq ft	74.8	4.670
Vertical-tail area (exposed), sq ft	48.0	3.000
Rudder area (including overhang), sq ft	11.39	0.712
<u>Fuselage</u>		
Length, ft	62.0	15.049
Maximum width, ft	4.375	1.094
Maximum height (excluding canopy), ft	6.50	1.625
Volume (including canopy), cu ft	1142	17.87
Location of station 0 (measured upstream from nose of airplane), in.	39.672	9.918
Side area (excluding vertical tail), sq ft	346	21.6
Frontal area (including canopy), sq ft	24.7	1.542

TABLE I.- DESIGN CHARACTERISTICS OF THE REPUBLIC F-105 AIRPLANE AND THE 1/4-SCALE MODEL OF THE F-105 AIRPLANE - CONCLUDED

10

	Full-scale	1/4-scale
<u>Trailing-Edge Flaps</u>		
Basic data:		
Type	Single slotted	Single slotted
Deflection, measured in a plane normal to 0.82c line, deg	0 to 46.2	0,30,35,40,46
Dimensions (maximum span flap):		
Average chord, measured parallel to airplane center line	0.25c	0.25c
Span (one flap), measured normal to airplane center line, ft	11.7	2.925
Location of outboard edge, measured normal to airplane center line, in.	168.0	42
Location of inboard edge, measured normal to airplane center line, in.	27.85	6.963
Area (maximum span flap):		
Area of both trailing-edge flaps, sq ft	69.6	4.35
<u>Leading-Edge Flaps</u>		
Basic data:		
Type	Drooped nose	Drooped nose
Deflection, measured in a plane normal to hinge line, deg	0 to 20	0,7.5,15,20,25,30
Location of inboard edge, measured normal to airplane center line, in.	82.149	20.537
Location of outboard edge, measured normal to airplane center line, in.	199.78	49.945
Dimensions:		
Average leading-edge flap chord (streamwise)	0.12c	0.12c
Span (one flap), measured normal to airplane center line, ft	9.8	2.45
Area:		
Area of both leading-edge flaps, sq ft	22.7	1.419
<u>External Tanks (450-gallon capacity)</u>		
Length, in.	227.55	56.89
Diameter (max.), in.	29.0	7.25
Angle of incidence, relative to fuselage center line, deg	-3.0	-3.0
Spanwise location, measured from fuselage center line, in.	129.0	31.75
Vertical location of nose of tank, measured below fuselage center line, in.	-40.04	-10.01
Longitudinal location of nose of tank, measured from fuselage station 0, in.	391.16	97.79

TABLE II.- SUMMARY OF THE LONGITUDINAL STABILITY CHARACTERISTICS OF A 1/4-SCALE
MODEL OF THE F-105 AIRPLANE WITH A TAIL ASPECT RATIO OF 3.06
AND A SUPERSONIC ELLIPTICAL INLET

Wing, aspect ratio	3.18	Fuselage basic
Tail, aspect ratio	3.06	Inlet supersonic-type elliptical

Wing configuration		Speed-brake deflection		Store	Tail configuration		C_L at $\alpha=12^\circ$	C_L max	α at C_L max	$(C_m$ characteristics about 0.25°)	Fig.
T.E. device	Stall-control device	Horiz-ontal, deg	Vert-ical, deg		Height 2z/b	NACA airfoil section	i_t , deg				
None	None	0	0	None	-0.123	65A series	off 0	0.63 0.70	0.95 1.15	26.7 26.8	6
single slotted flap $0.133b/2$ to $0.600b/2$ $\delta = 46^\circ$	L.E. flap $0.382b/2$ to $0.950b/2$ $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-7.3 3.5 7.0	0.99 1.01 1.08	1.20 1.21 1.35	20.6 19.4 19.4	8
single slotted flap $0.133b/2$ to $0.650b/2$ $\delta = 46^\circ$	L.E. flap $0.382b/2$ to $0.950b/2$ $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-7.3 3.5 7.0	1.01 1.06 1.08	1.21 1.29 1.35	19.4 19.8 19.4	9
single slotted flap $0.133b/2$ to $0.700b/2$ $\delta = 46^\circ$	L.E. flap $0.382b/2$ to $0.950b/2$ $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-7.3 3.5 7.0	1.02 1.05 1.14	1.22 1.26 1.34	28.0 28.6* 20.0	10
single slotted flap $0.133b/2$ to $0.700b/2$ $\delta = 46^\circ$	L.E. flap $0.382b/2$ to $0.950b/2$ $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-9.7 -7.3 0.1 3.5	1.02 1.05 1.13 1.15	1.22 1.27 1.20 1.33	25.0 29.0* 18.4 19.8	11

* Highest angle of test.

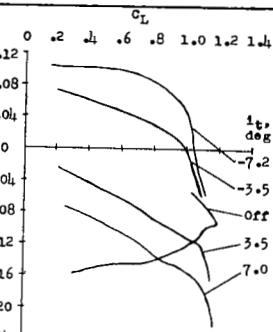
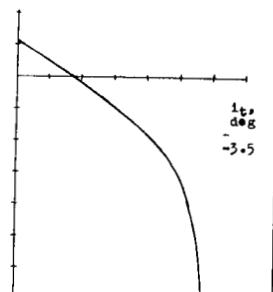
TABLE II-- SUMMARY OF THE LONGITUDINAL STABILITY CHARACTERISTICS OF A 1/4-SCALE
MODEL OF THE F-105 AIRPLANE WITH A TAIL ASPECT RATIO OF 3.06
AND A SUPERSONIC ELLIPTICAL INLET - Continued

Wing configuration		Speed-brake deflection	Store	Tail configuration			C_L at $\alpha=12^\circ$	C_L max	α at C_L max	C_m characteristics about 0.25c	Fig.
T.E. device	Stall-control device			Horizontal, deg	Vertical, deg	Height 2z/b	NACA airfoil section				
Single slotted flap 0.135a/2 to 0.800a/2 $\delta = 46^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-14.3	1.05	1.20	24.0*	24
Single slotted flap 0.135a/2 to 0.800a/2 $\delta = 46^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 30^\circ$	0	0	450 gal	-0.123	65A series	-14.3	1.16	1.32	21.0	14
Single slotted flap 0.135a/2 to 0.800a/2 $\delta = 46^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 30^\circ$	0	0	450 gal	-0.123	65A series	-9.7	1.18	1.32	21.6	15
Single slotted flap 0.135a/2 to 0.800a/2 $\delta = 40^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 30^\circ$	0	0	450 gal	-0.123	65A series	-3.4	1.14	1.41	21.0	16
Single slotted flap 0.135a/2 to 0.700a/2 $\delta = 40^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	0.1	1.16	1.42	21.5	17
Single slotted flap 0.135a/2 to 0.700a/2 $\delta = 40^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-14.3	0.98	1.30	24.0	18
Single slotted flap 0.135a/2 to 0.700a/2 $\delta = 40^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-9.7	1.03	1.37	23.0	19
Single slotted flap 0.135a/2 to 0.700a/2 $\delta = 40^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-3.5	1.07	1.44	23.4	20
Single slotted flap 0.135a/2 to 0.700a/2 $\delta = 40^\circ$	L.E. flap 0.382b/2 to 0.950b/2 $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	0.1	1.12	1.44	23.0	21

* Highest angle of test.

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TABLE II.- SUMMARY OF THE LONGITUDINAL STABILITY CHARACTERISTICS OF A 1/4-SCALE
MODEL OF THE F-105 AIRPLANE WITH A TAIL ASPECT RATIO OF 3.06
AND A SUPERSONIC ELLIPTICAL INLET - Concluded

Wing configuration		Speed-brake deflection	Store	Tail configuration			C_L at $\alpha=12^\circ$	$C_{L\max}$	α at $C_{L\max}$	C_m characteristics about $0.25C_L$	Fig.	
T.E. device	Stall-control device	Horizontal, deg		Vertical, deg	Height 2z/b	NACA airfoil section						
Single slotted flap $0.135b/2$ to $0.650b/2$ $\delta = 40^\circ$	L.E. flap $0.382b/2$ to $0.950b/2$ $\delta = 20^\circ$	0	0	450 gal	-0.123	65A series	-7.2 -3.5 3.5 7.0	0.96 0.99 1.05 1.10	1.22 1.28 1.19 1.39	29.0* 21.4 18.6 21.0		20 21
None	L.E. flap $0.382b/2$ to $0.950b/2$ $\delta = 7.5^\circ$	0	0	None	-0.123	65A series	-3.5	0.66	1.16	28.6		26

* Highest angle of test.

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TABLE III.- SUMMARY OF THE LONGITUDINAL STABILITY CHARACTERISTICS OF A 1/4-SCALE MODEL OF THE F-105 AIRPLANE WITH A TAIL ASPECT RATIO OF 3.06 AND A TRANSONIC ELLIPTICAL INLET

Wing, aspect ratio	3.18	Fuselage basic
Tail, aspect ratio	3.06	Inlet transonic-type elliptical

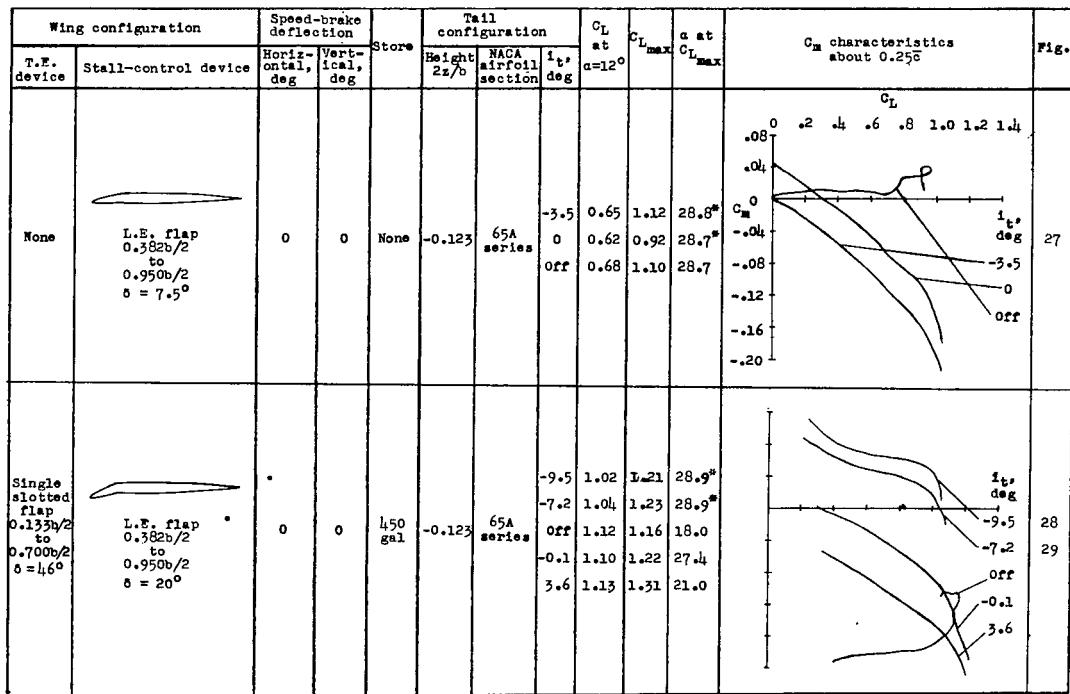
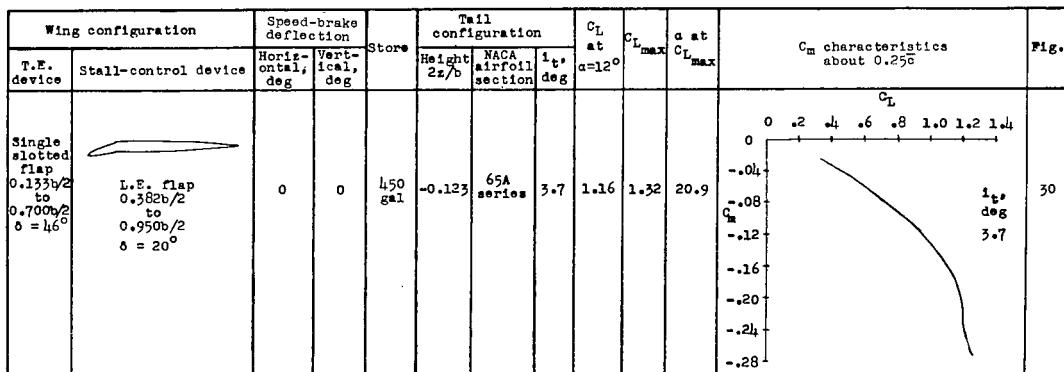


TABLE IV.- SUMMARY OF THE LONGITUDINAL STABILITY CHARACTERISTICS OF A 1/4-SCALE MODEL OF THE F-105 AIRPLANE WITH A TAIL ASPECT RATIO OF 3.49 AND A TRANSONIC ELLIPTICAL INLET

Wing, aspect ratio	3.18	Fuselage basic
Tail, aspect ratio	3.49	Inlet transonic-type elliptical



*Highest angle of test

CONT

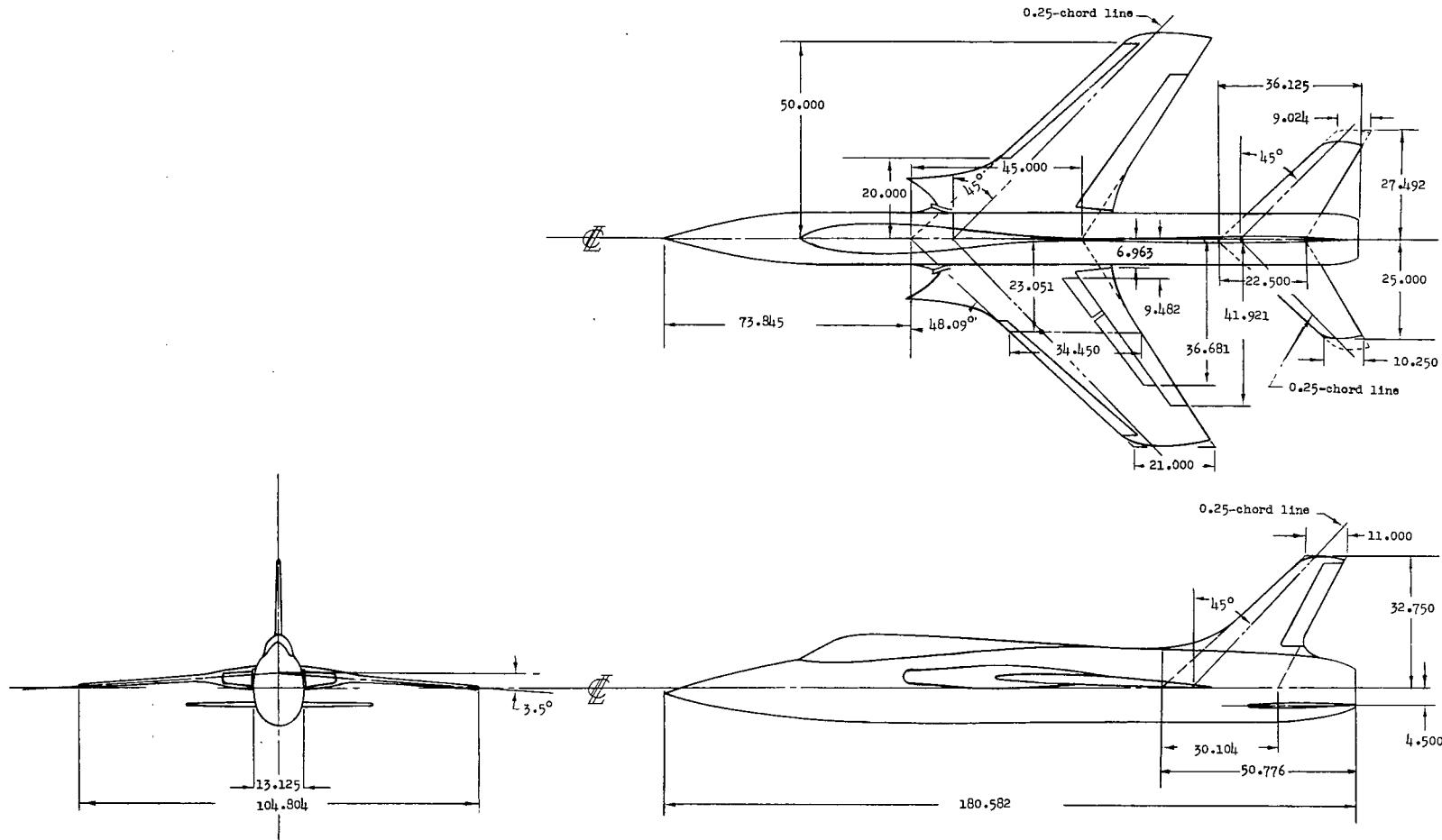


Figure 1.- Three-view drawing of a 1/4-scale model of the F-105 airplane.
(Dimensions in inches unless otherwise noted.)

NACA RM SL54H27

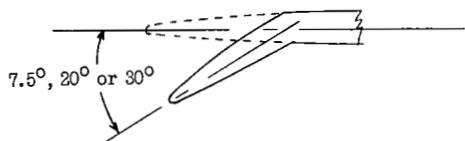
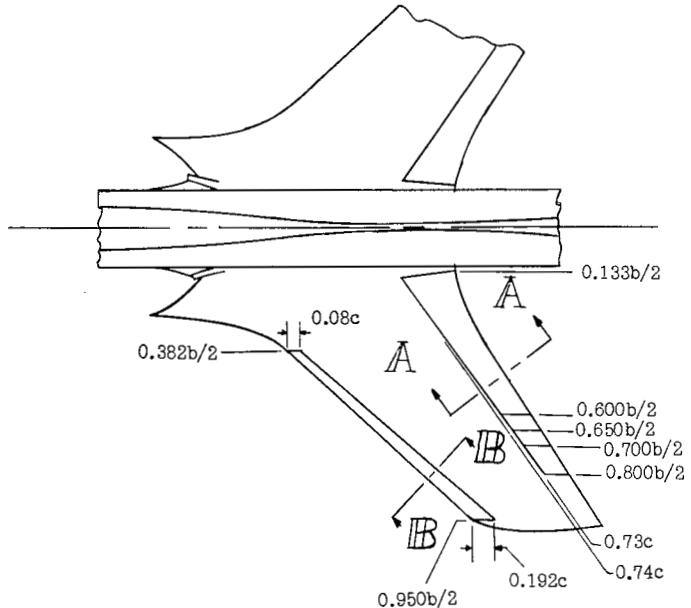
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L-84117

Figure 2.- The 1/4-scale model of the F-105 airplane mounted on the normal three-support system of the Langley 19-foot pressure tunnel.

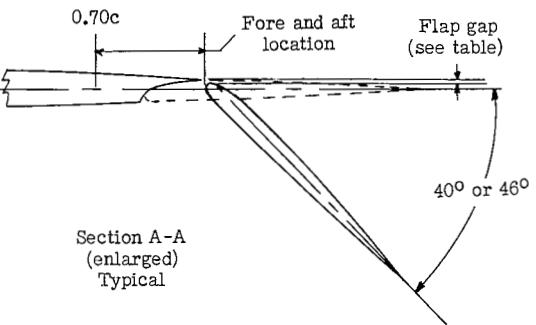
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Section B-B
(enlarged)
Typical

(a) Leading-edge flap.

Flap station $b/2$	Deflection			Flap gap, inches			Fore and aft position, inches		
	Actual		Loft	Actual		Loft	Actual		Loft
	L.H.	R.H.		L.H.	R.H.		L.H.	R.H.	
0.242	46°49'	46°26'	46°13'	0.41	0.40	0.415	2.72	2.73	2.72
.415	46°42'	46°45'	46°13'	.31	.32	.350	2.92	2.91	2.90
.647	46°34'	46°54'	46°13'	--	--	--	--	--	--
.869	--	--	--	.345	.34	.295	2.45	2.47	2.47



Section A-A
(enlarged)
Typical

(b) Trailing-edge flap.

Figure 3.- Details of the leading- and trailing-edge flaps.

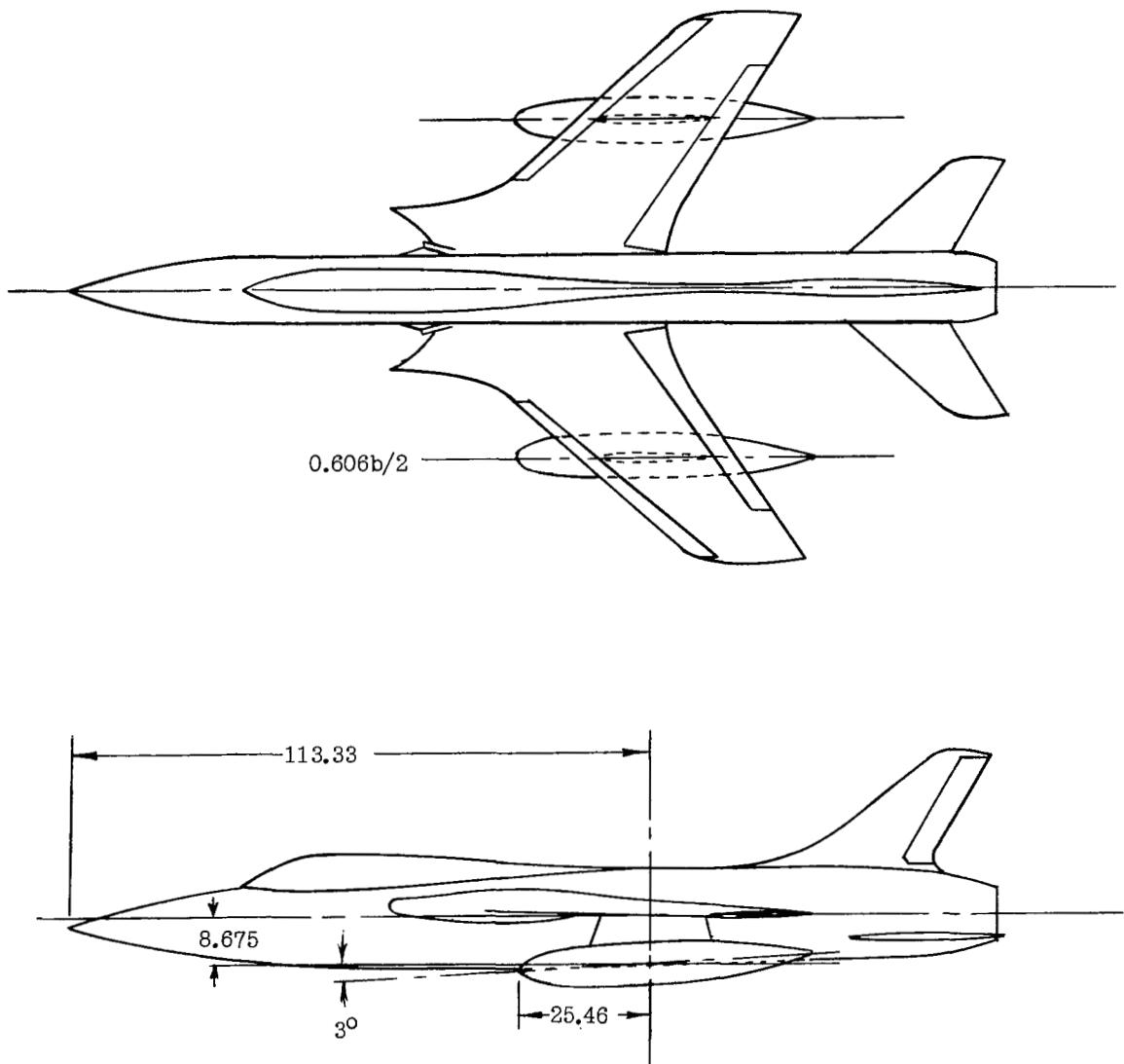
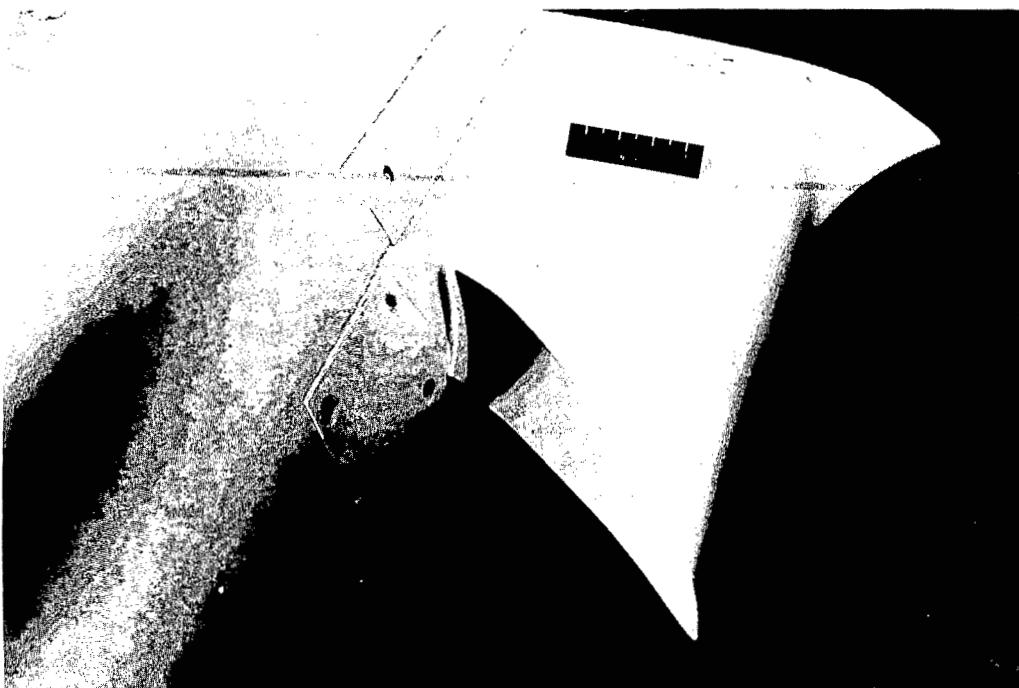
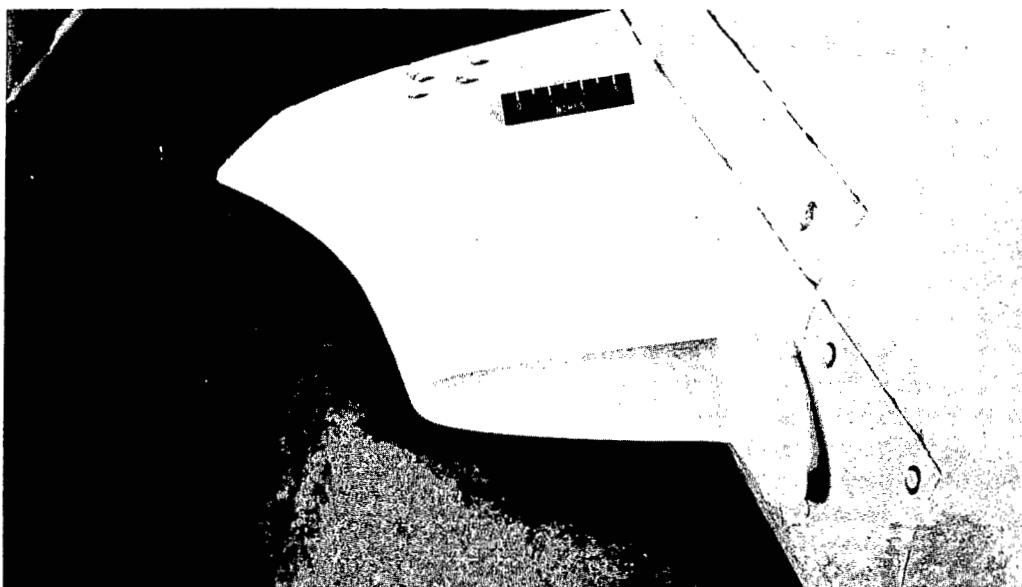


Figure 4.- Details of the external stores. (All dimensions in inches).



(a) Supersonic-type elliptical inlet.

L-85123



(b) Transonic-type elliptical inlet.

L-85124

Figure 5.- Wing-root inlets of the 1/4-scale model of the F-105 airplane
(without wing).

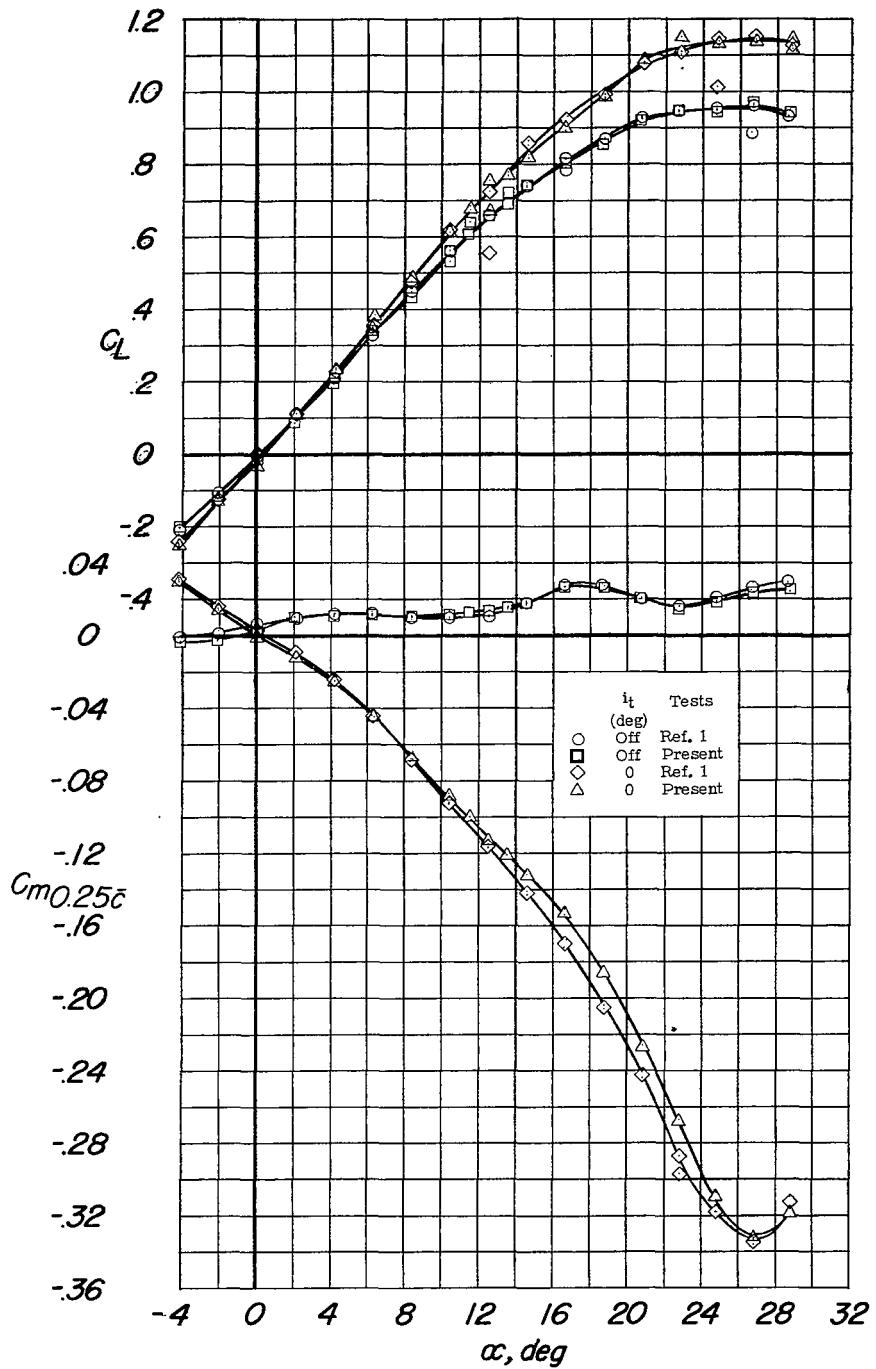
(a) C_L and $C_{m0.25c}$ against α .

Figure 6.- Longitudinal characteristics of the model obtained during the present tests and the tests of reference 1. Configuration: A + V + I_{SE} + (-0.123)T; center-of-gravity location, 0.25c.

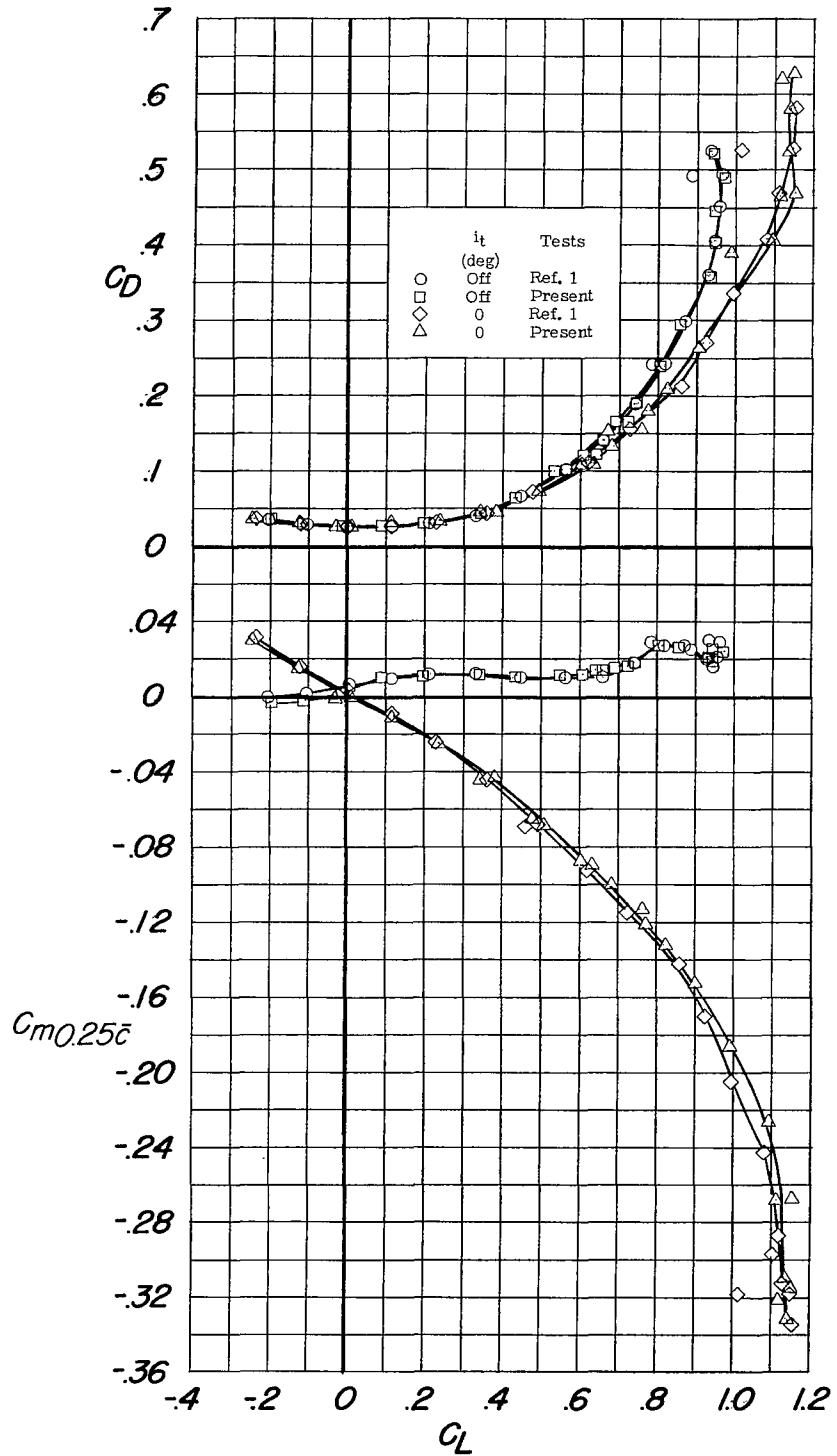
(b) C_D and $C_{m,0.25c}$ against C_L .

Figure 6.- Concluded.

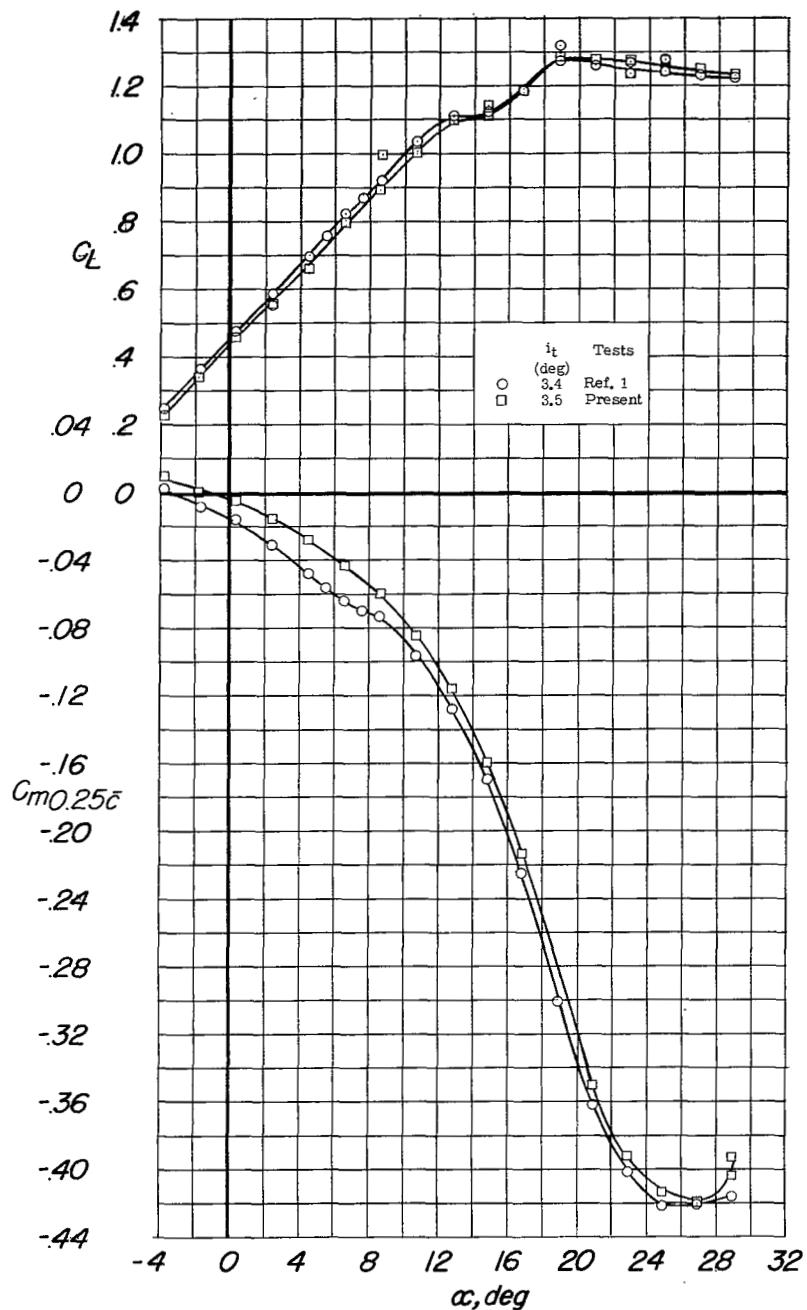
(a) C_L and $C_{m0.25c}$ against α .

Figure 7.- Longitudinal characteristics of the model with 60-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° obtained during the present tests and the tests of reference 1. Configuration: A + V + I_{SE} + (-0.123)T + 0.60F₄₆ + N₂₀ + E₀⁴⁵⁰; center-of-gravity location, 0.25 c .

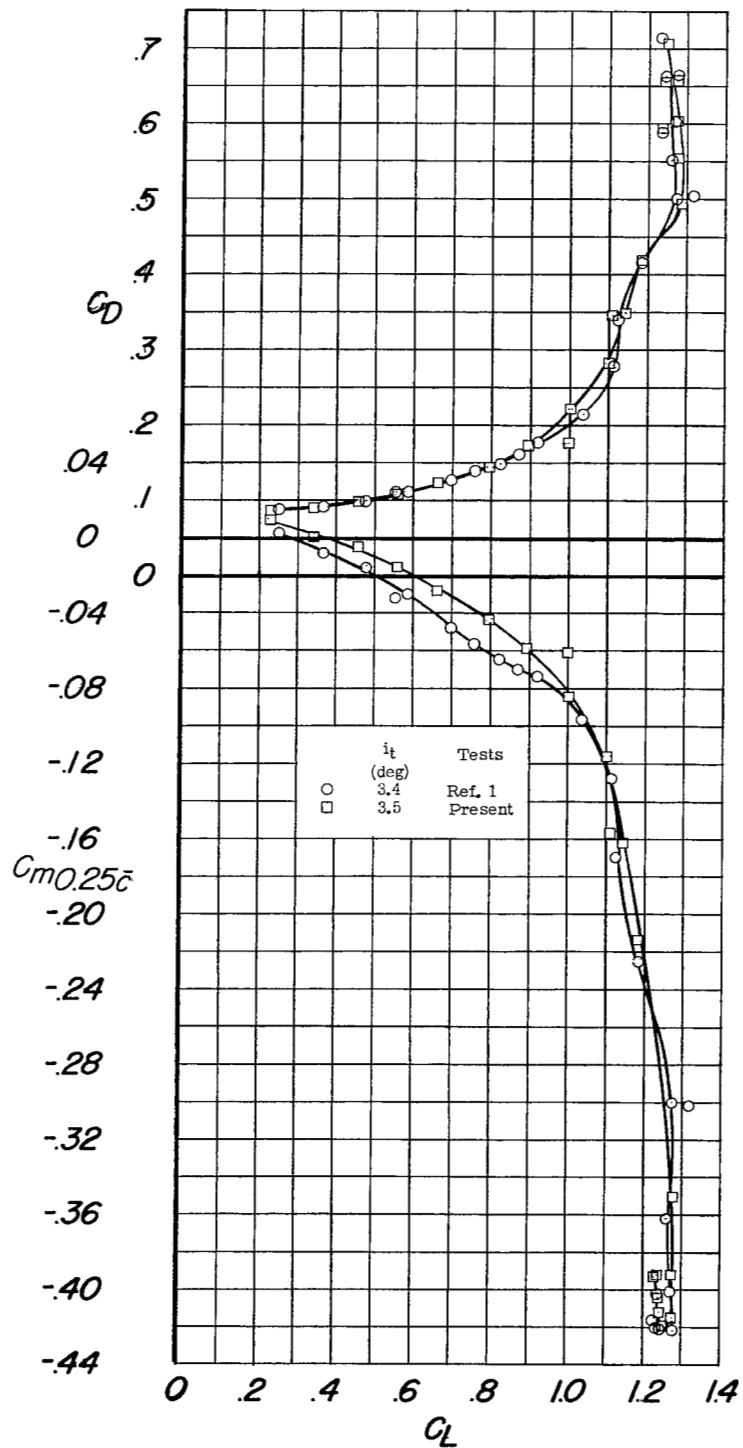
(b) C_D and $C_{m0.25c}$ against C_L .

Figure 7.- Concluded.

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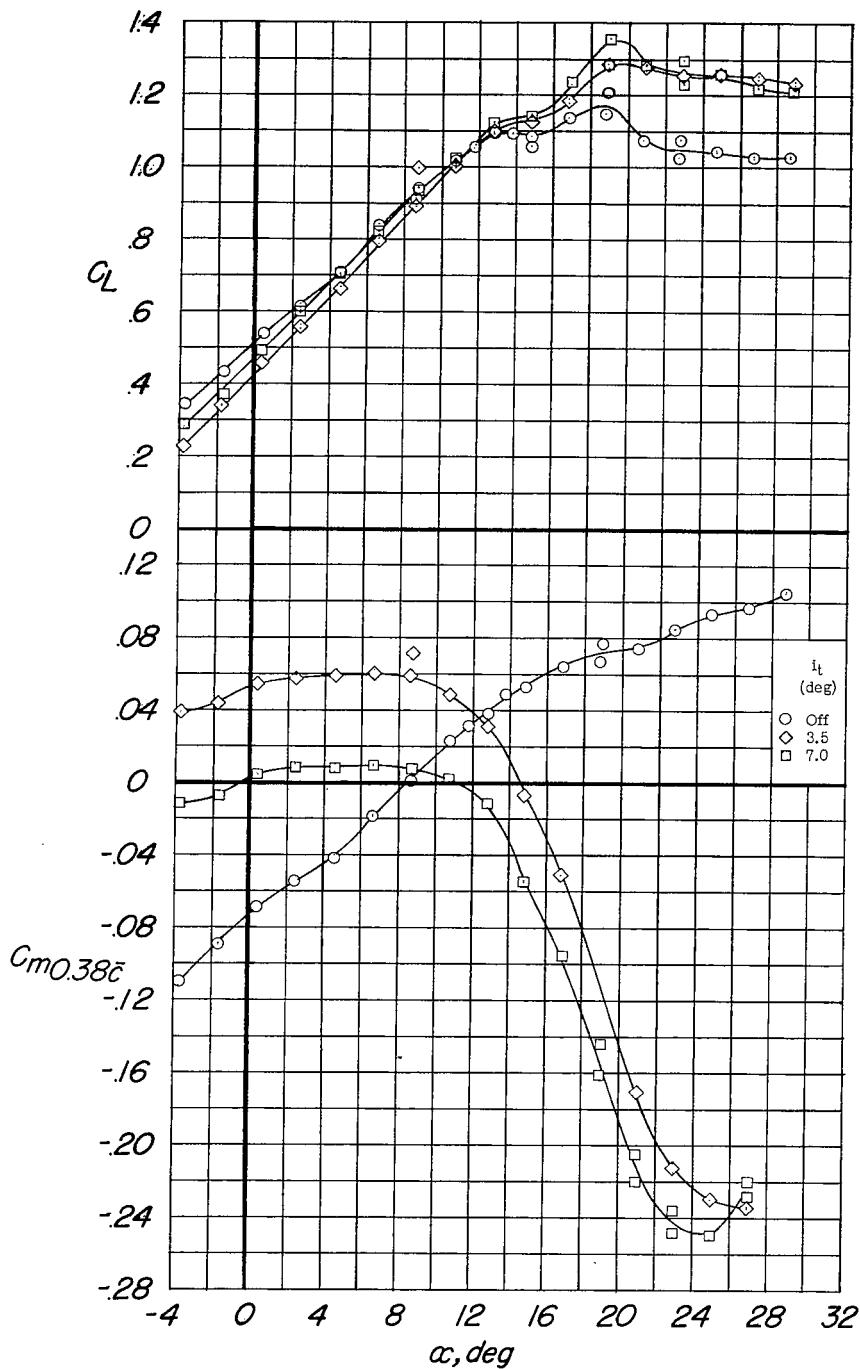
(a) C_L and $C_{m0.38c}$ against α .

Figure 8.- Longitudinal characteristics of the model with 60-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + ISE + $(-0.123)T + 0.60F46 + N_{20} + E_0^{450}$; center-of-gravity location, $0.38\bar{c}$.

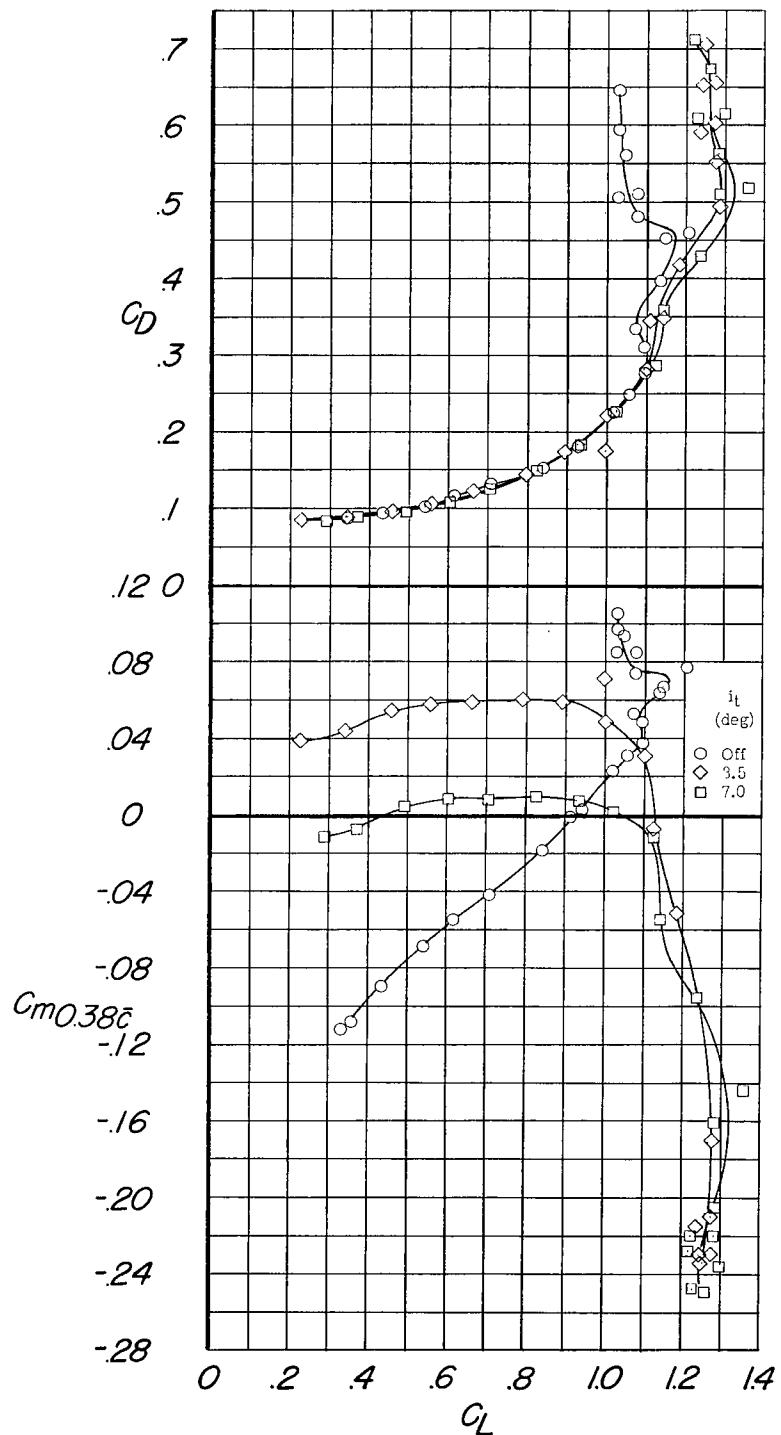
~~CONFIDENTIAL~~(b) C_D and $C_{m0.38\bar{c}}$ against C_L .

Figure 8.- Concluded.

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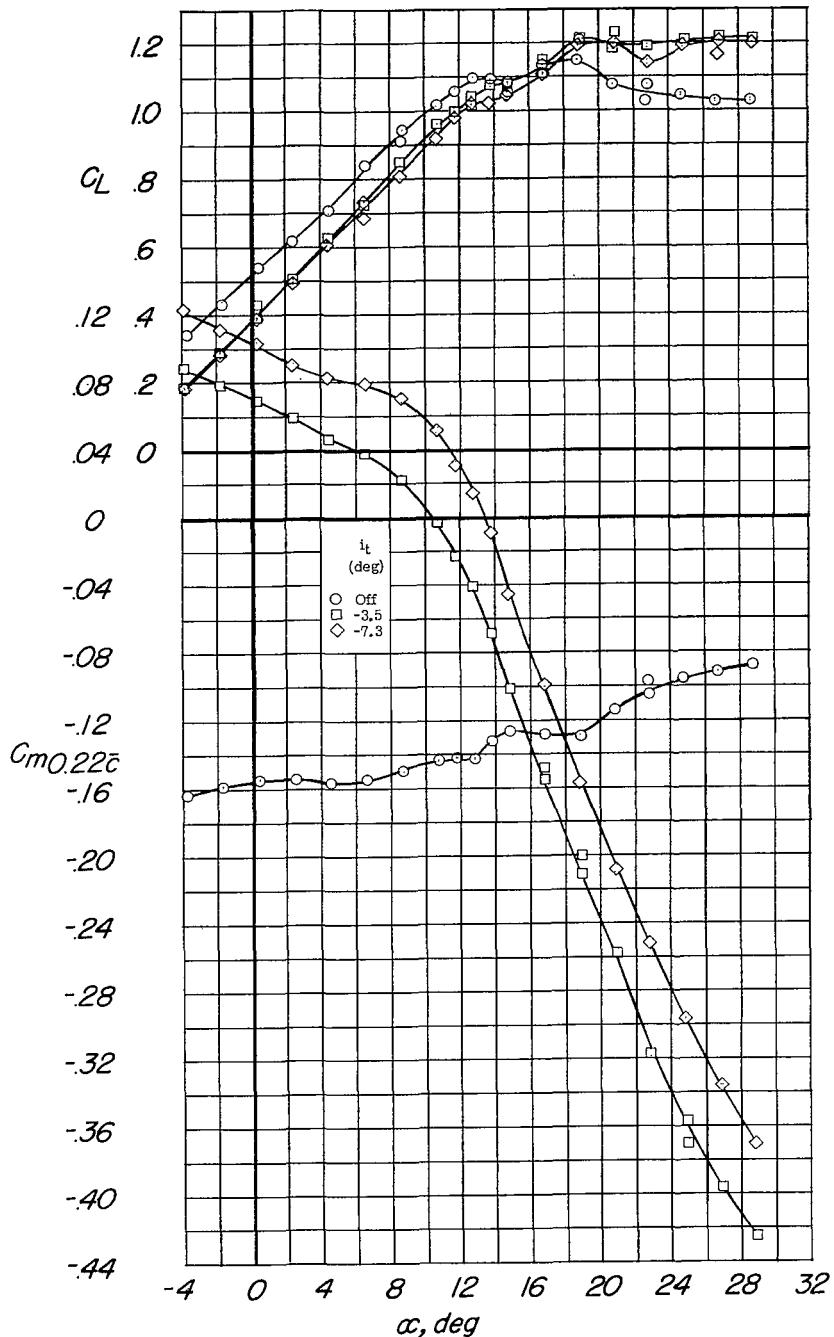
(a) C_L and $C_{m,0.22\bar{c}}$ against α .

Figure 9.- Longitudinal characteristics of the model with 60-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + ISE + $(-0.123)T + 0.60F_{46} + N_{20} + E_0^{450}$; center-of-gravity location, $0.22\bar{c}$.

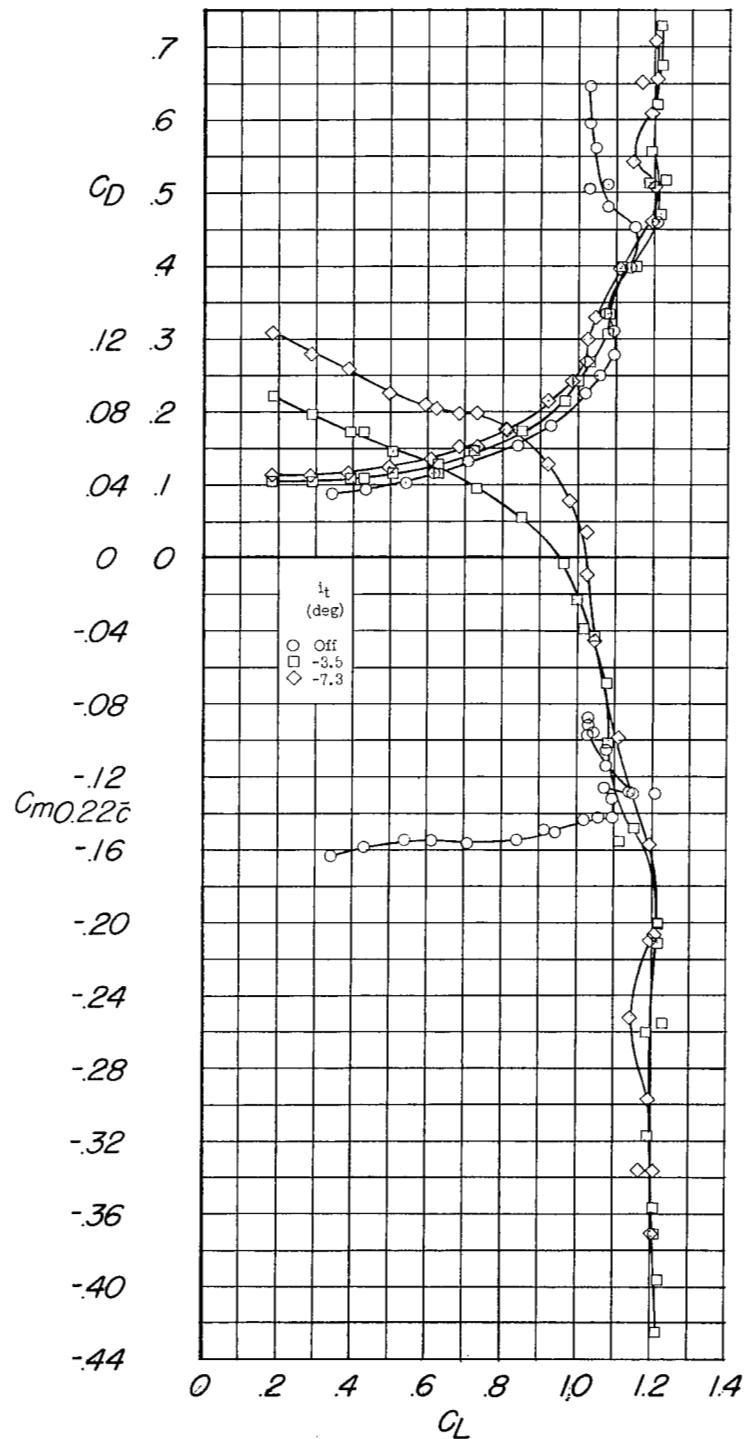
(b) C_D and $C_{m0.22\bar{c}}$ against C_L .

Figure 9.- Concluded.

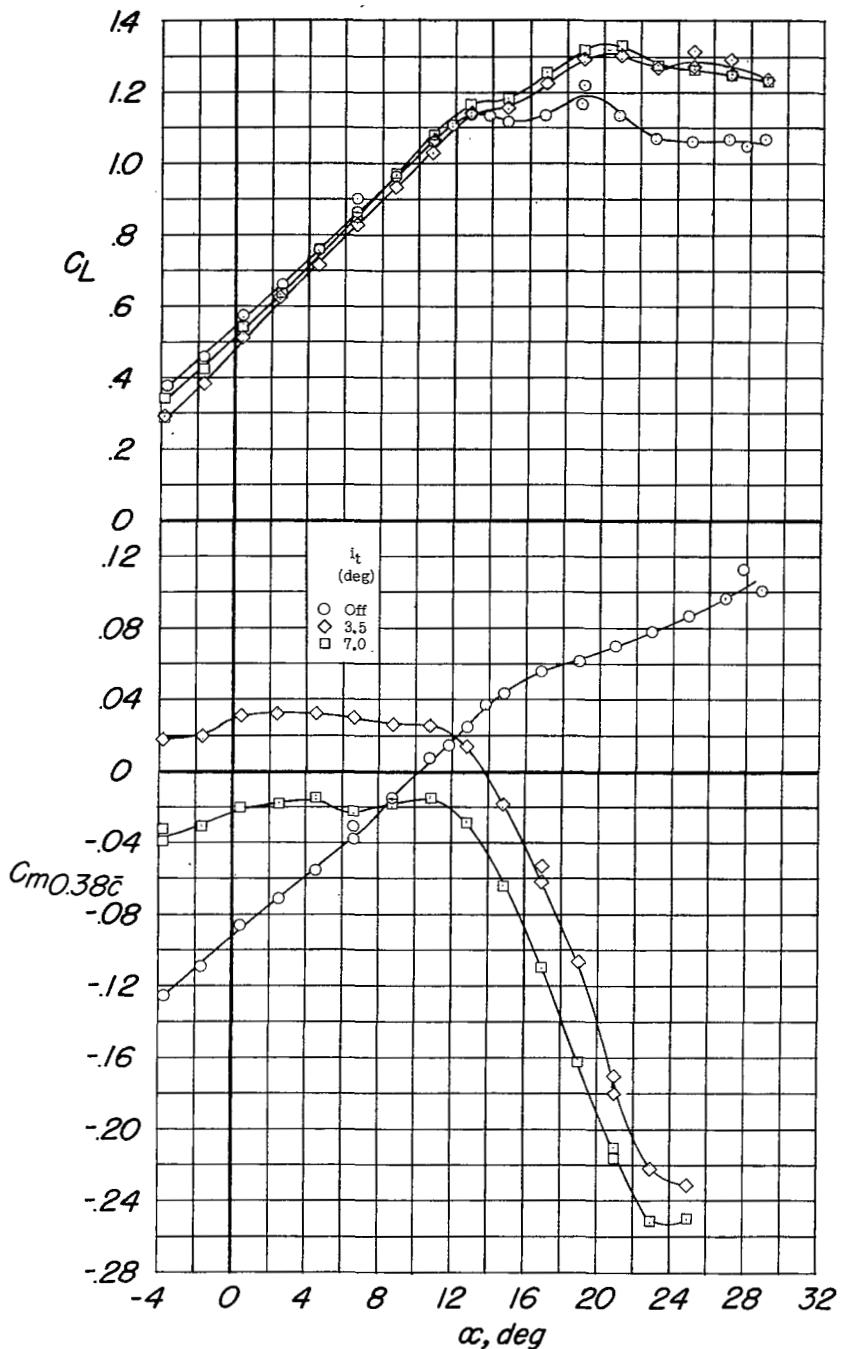
(a) C_L and $C_{m,0.38\bar{c}}$ against α .

Figure 10.- Longitudinal characteristics of the model with 65-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T + 0.65F₄₆ + N₂₀ + E₀₄₅₀; center-of-gravity location, $0.38\bar{c}$.

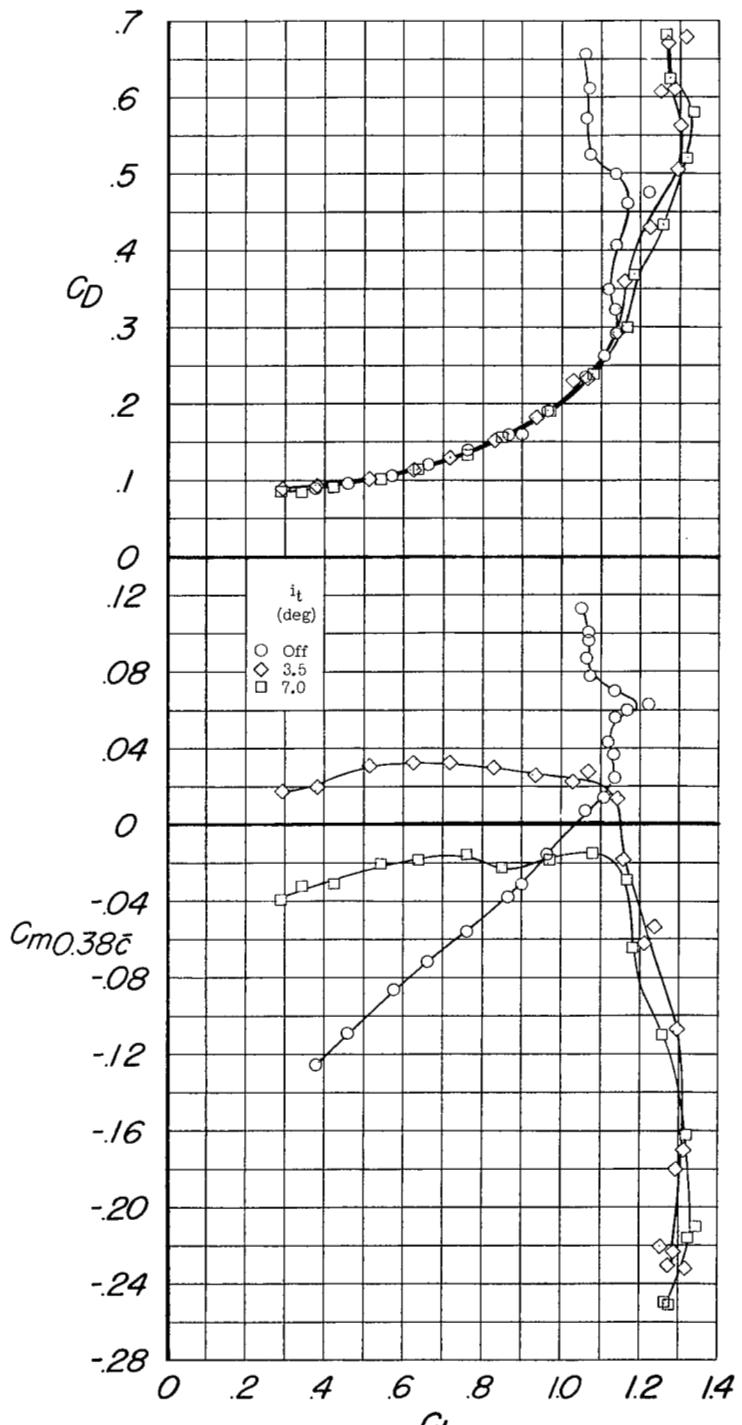
~~CONFIDENTIAL~~(b) C_D and $C_{m0.38\bar{c}}$ against C_L .

Figure 10.- Concluded.

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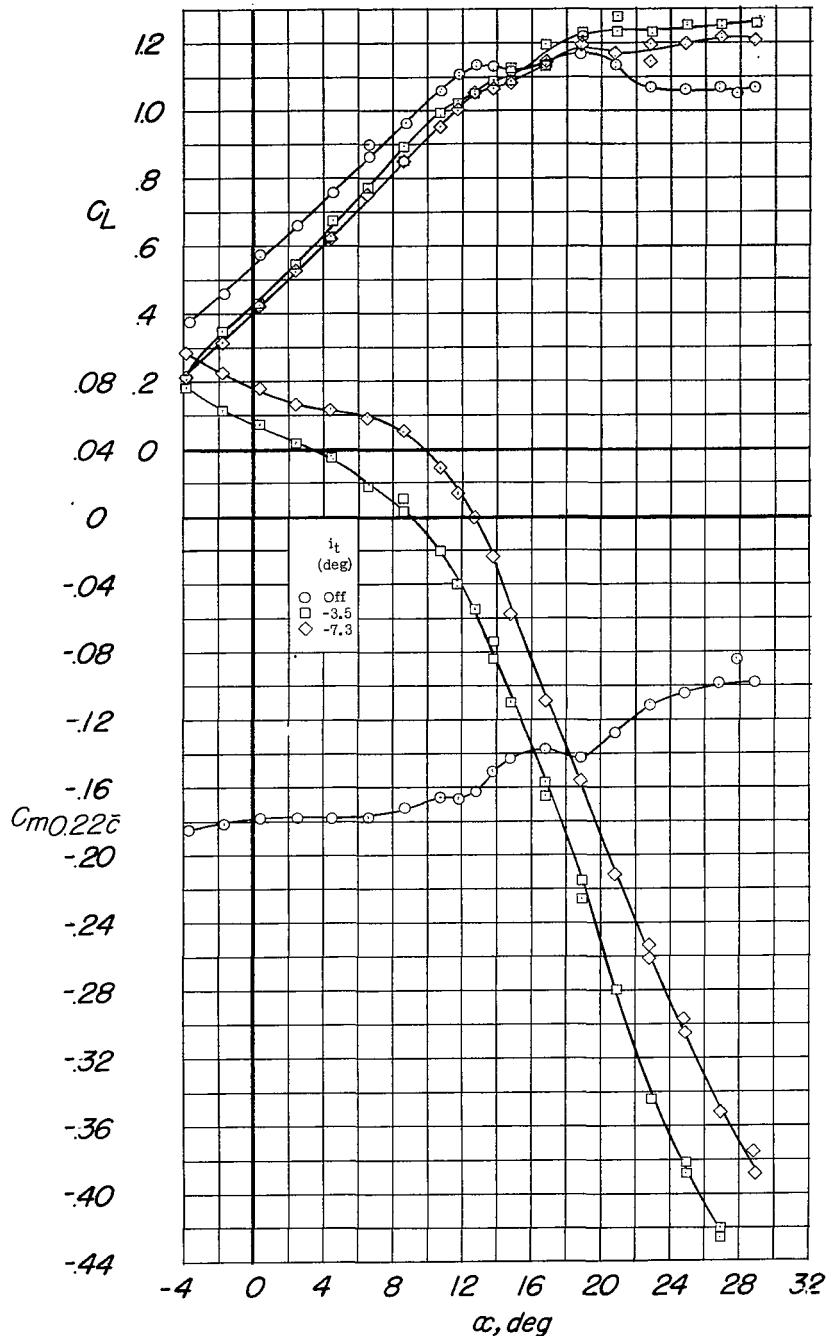
(a) C_L and $C_{m,0.22\bar{c}}$ against α .

Figure 11.- Longitudinal characteristics of the model with 65-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T + 0.65F₄₆ + N₂₀ + E₀⁴⁵⁰; center-of-gravity location, $0.22\bar{c}$.

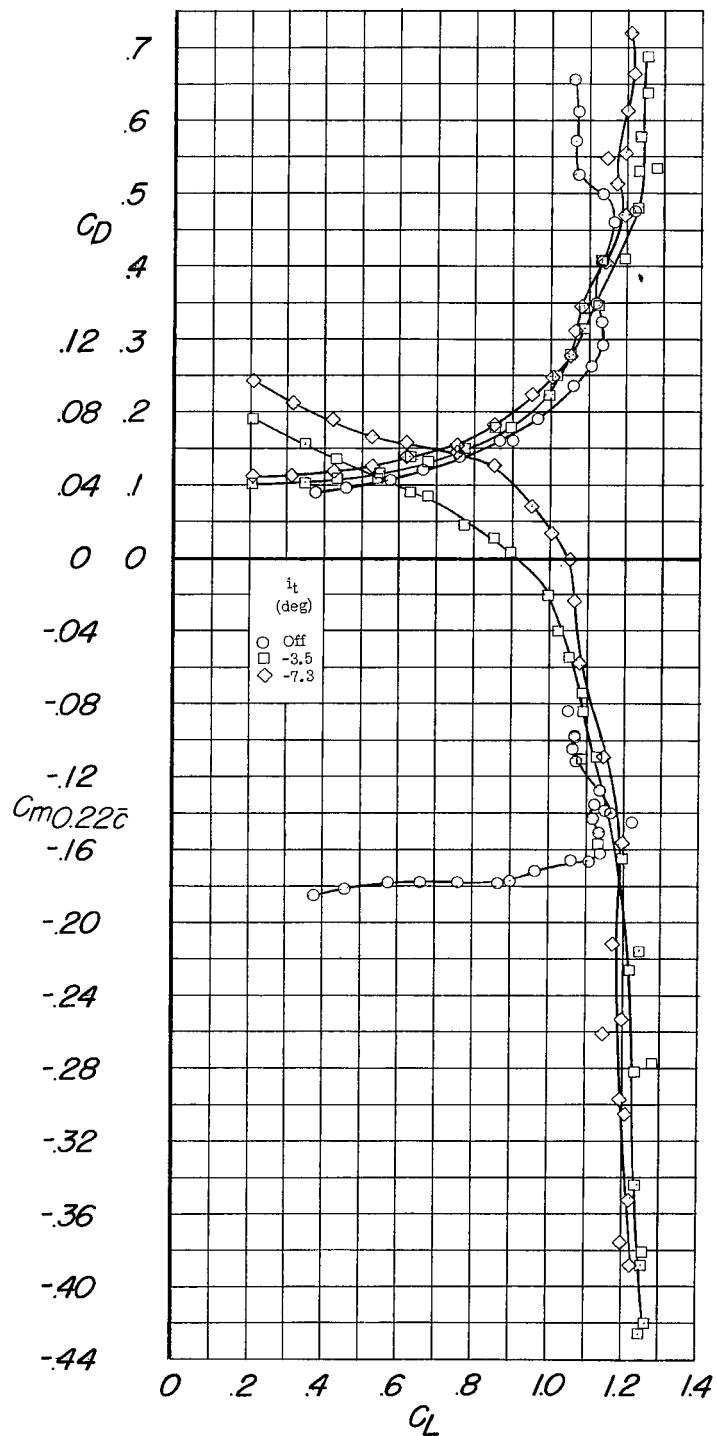
~~CONFIDENTIAL~~(b) C_D and $C_{m,0.22\bar{c}}$ against C_L .

Figure 11.- Concluded.

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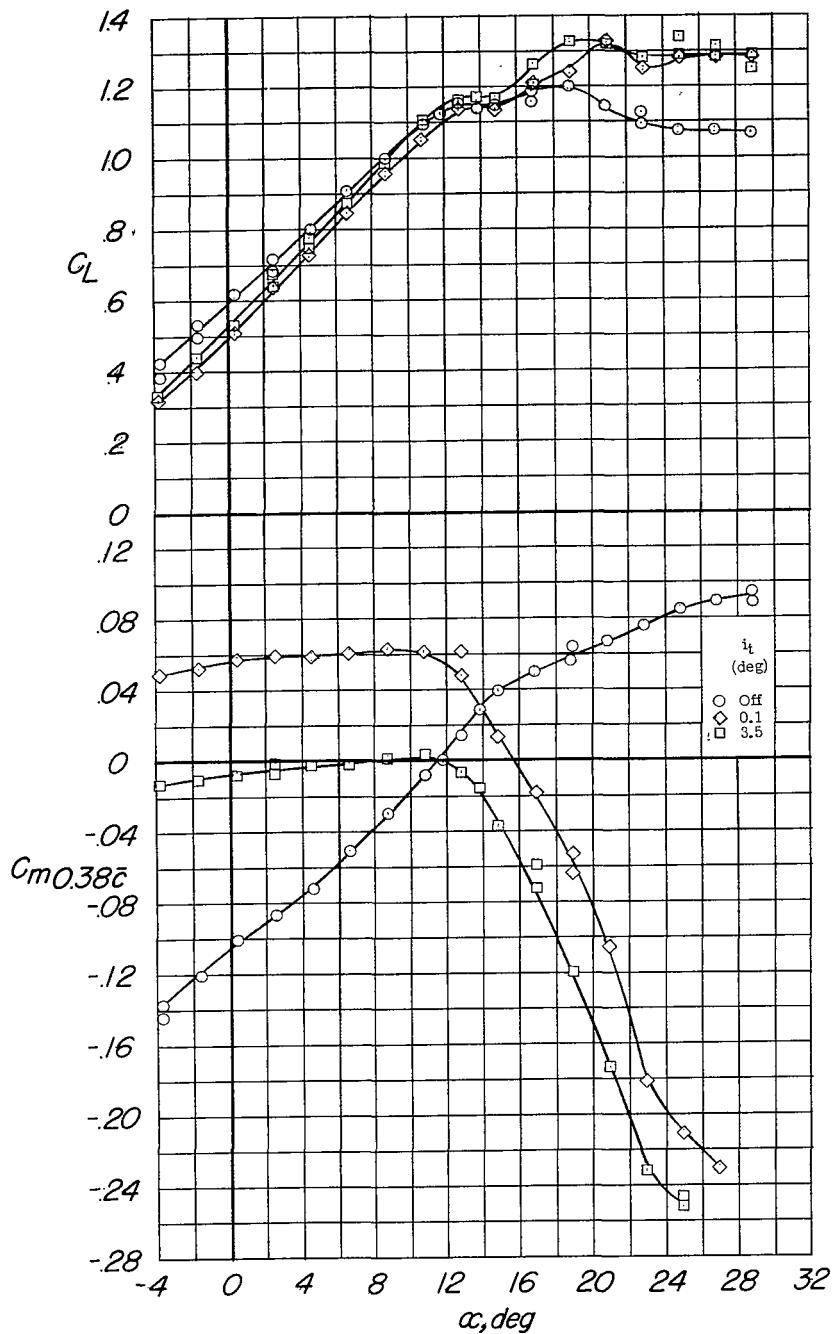
(a) C_L and $C_{m0.38\bar{c}}$ against α .

Figure 12.- Longitudinal characteristics of the model with 70-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T + 0.70F46 + N₂₀ + E₀450; center-of-gravity location, 0.38 \bar{c} .

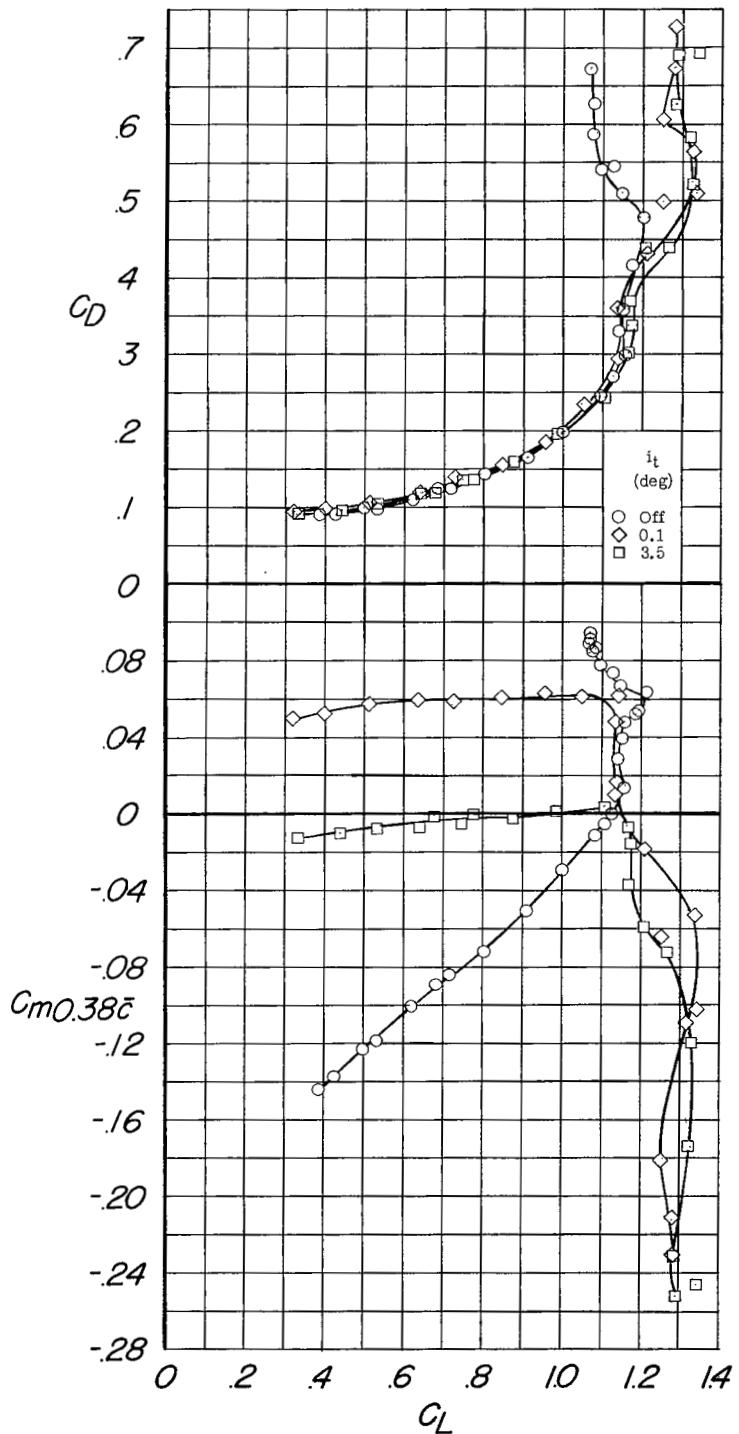
(b) C_D and $C_{m0.38\bar{c}}$ against C_L .

Figure 12.- Concluded.

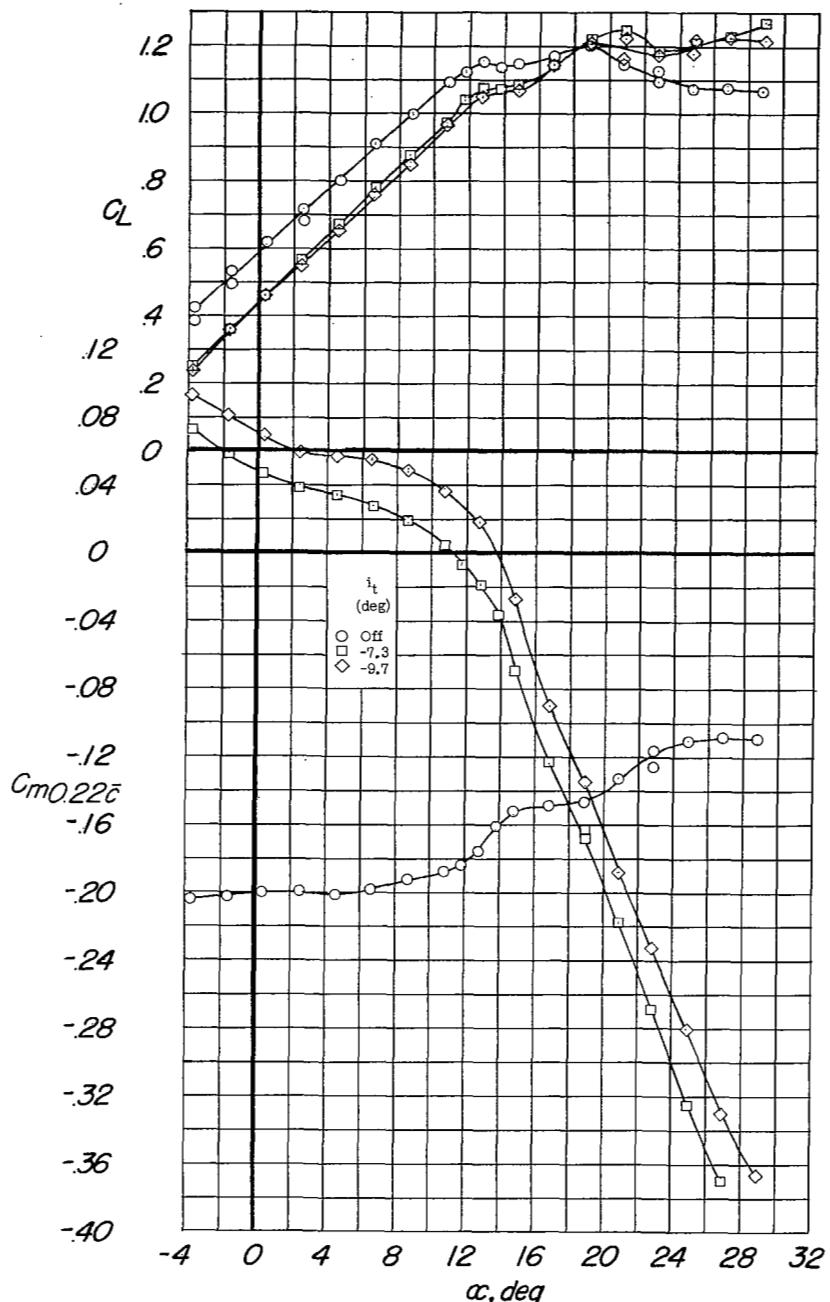
~~CONFIDENTIAL~~(a) C_L and $C_{m0.22\bar{c}}$ against α .

Figure 13.- Longitudinal characteristics of the model with 70-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T + 0.70F₄₆ + N₂₀ + E₀⁴⁵⁰; center-of-gravity location, $0.22\bar{c}$.

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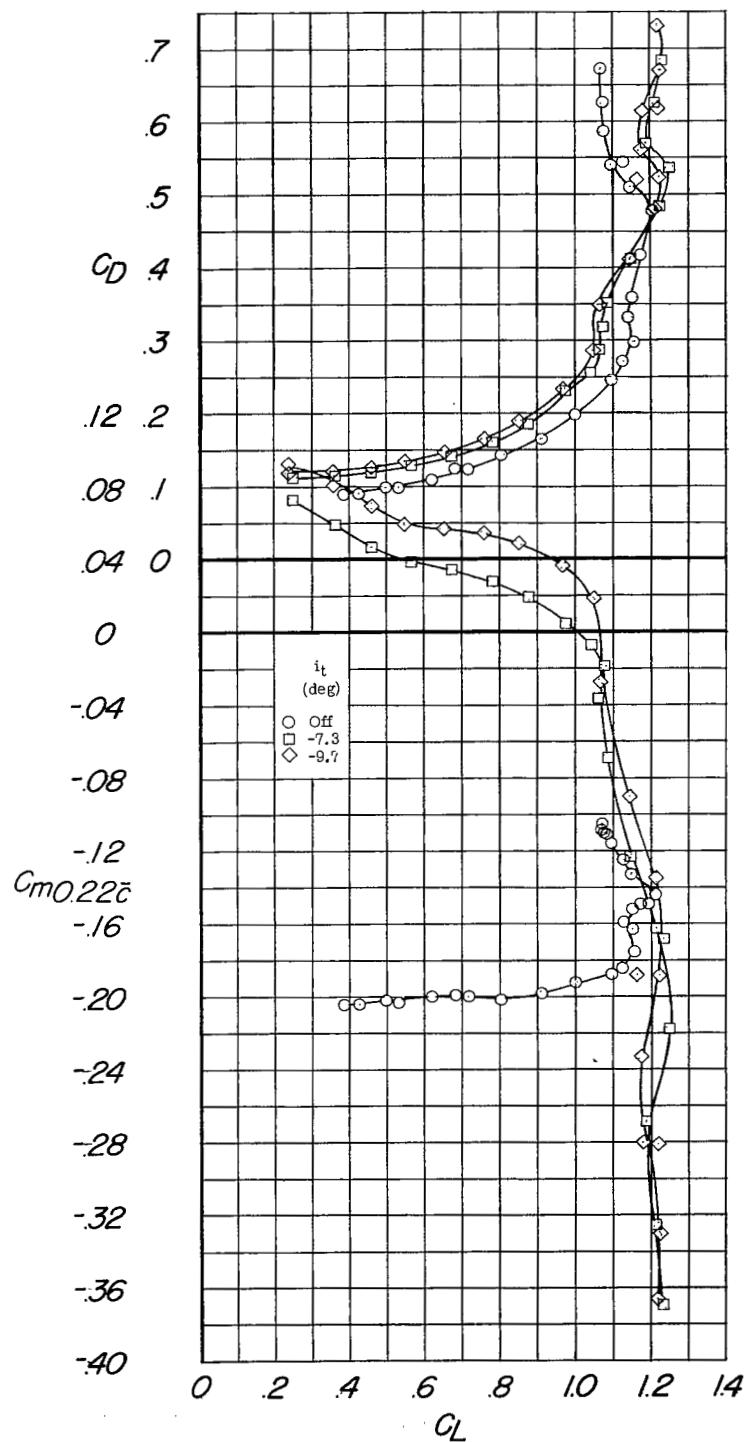
(b) C_D and $C_{m0.22\bar{c}}$ against C_L .

Figure 13.- Concluded.

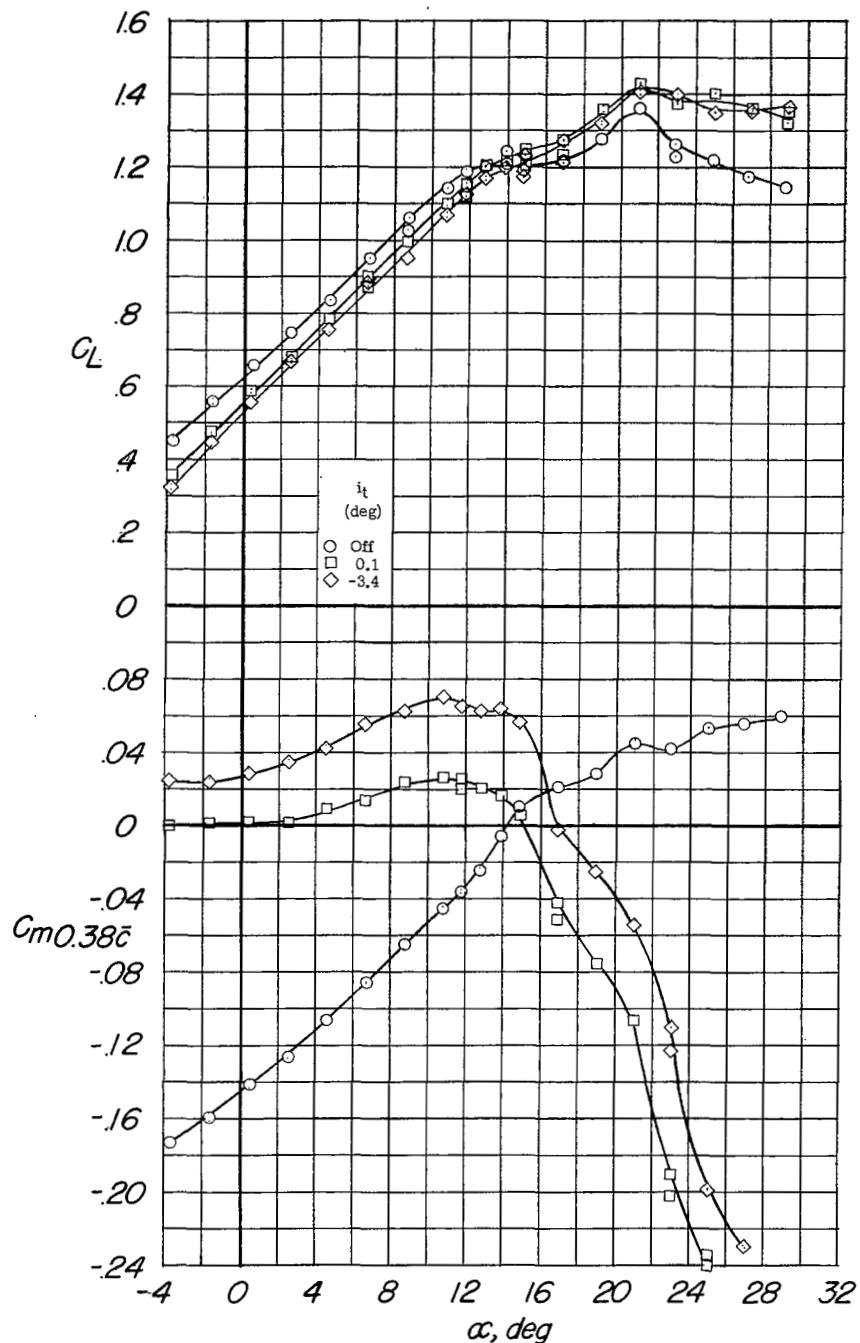
(a) C_L and $C_{m0.38\bar{c}}$ against α .

Figure 14.- Longitudinal characteristics of the model with 80-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 30° . Configuration: A + V + I_{SE} + (-0.123)T + 0.80F₄₆ + N₃₀ + E₀⁴⁵⁰; center-of-gravity location, $0.38\bar{c}$.

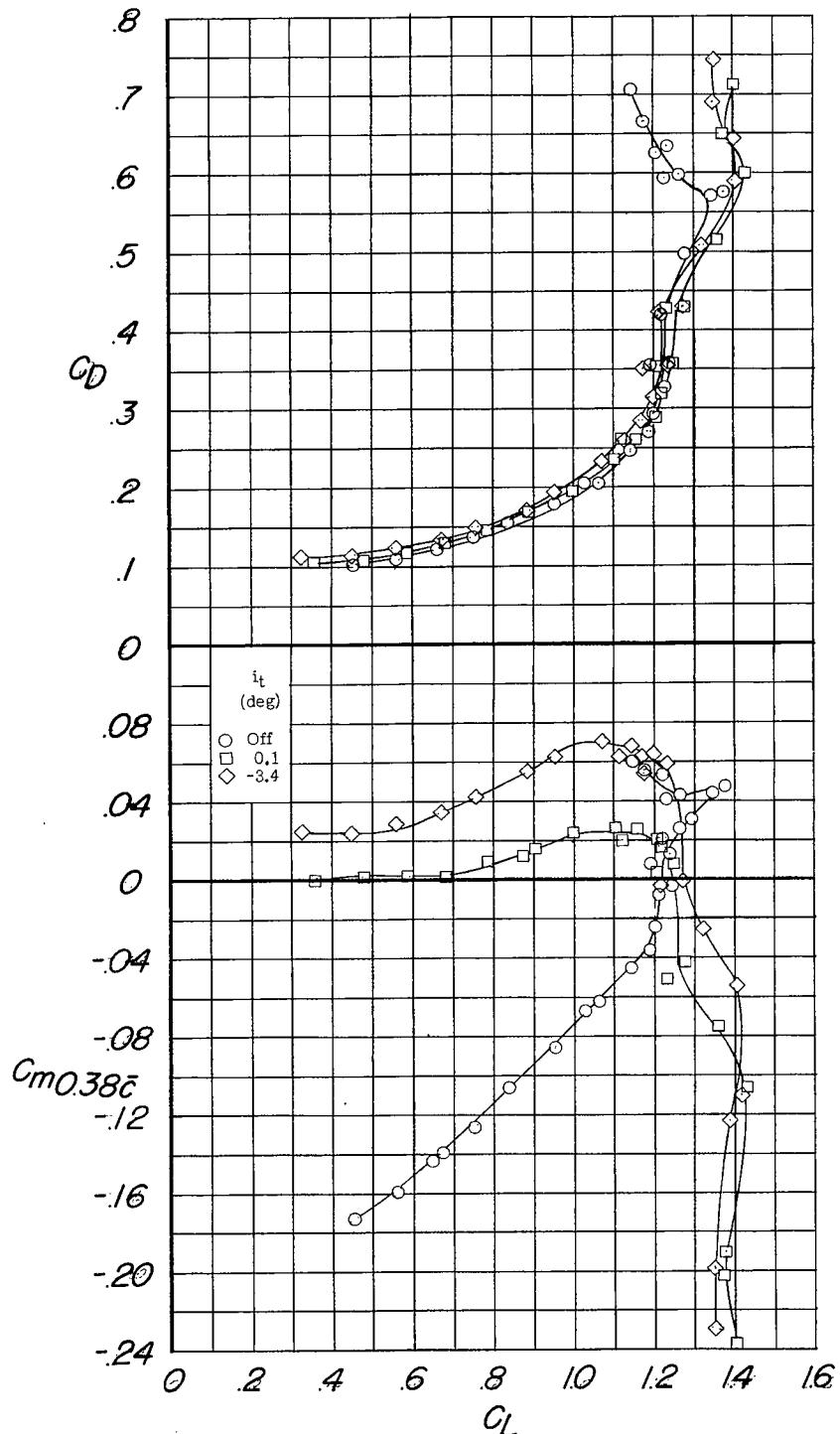
(b) C_D and $C_{m0.38\bar{c}}$ against C_L .

Figure 14.- Concluded.

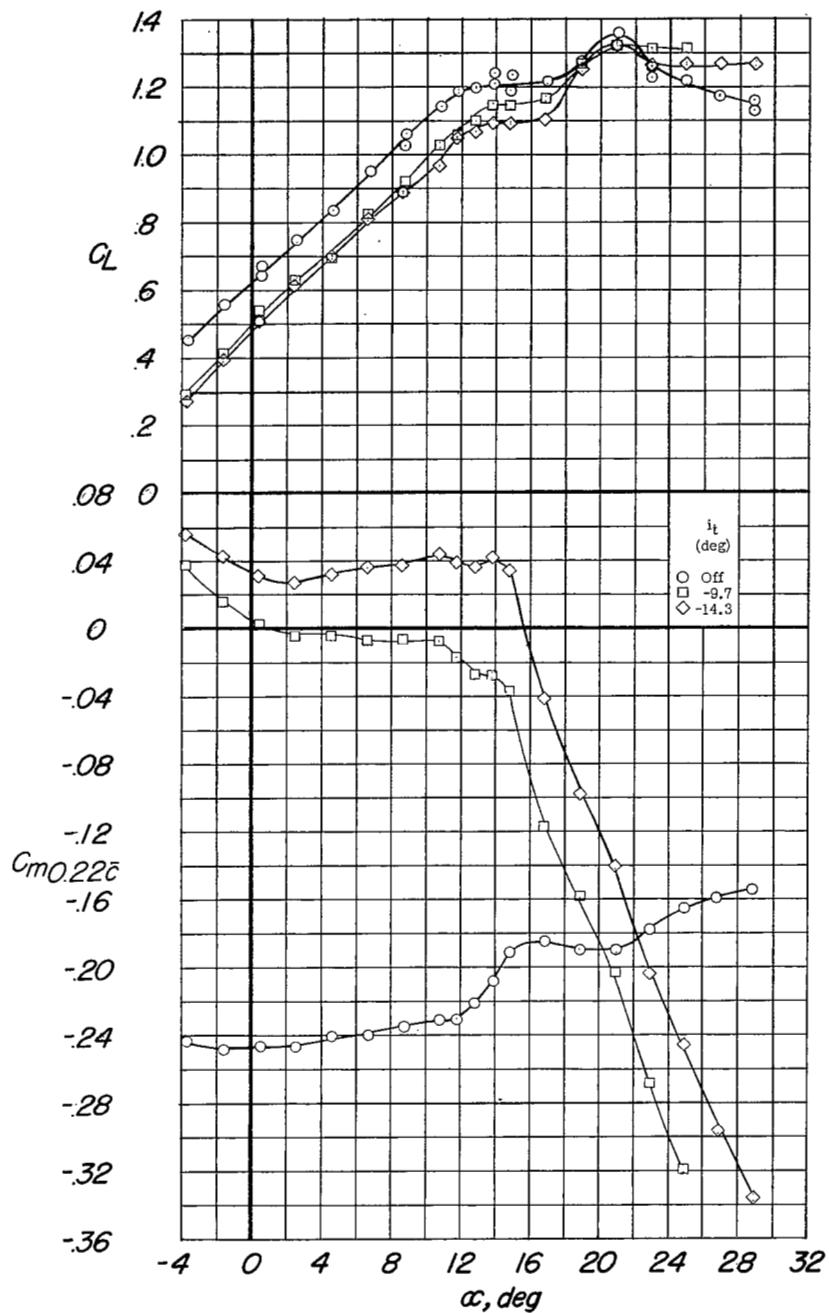
(a) C_L and $C_{m0.22\bar{c}}$ against α .

Figure 15.- Longitudinal characteristics of the model with 80-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 30° . Configuration: A + V + ISE + $(-0.123)T + 0.80F_{46} + N_{30} + E_0^{450}$; center-of-gravity location, $0.22\bar{c}$.

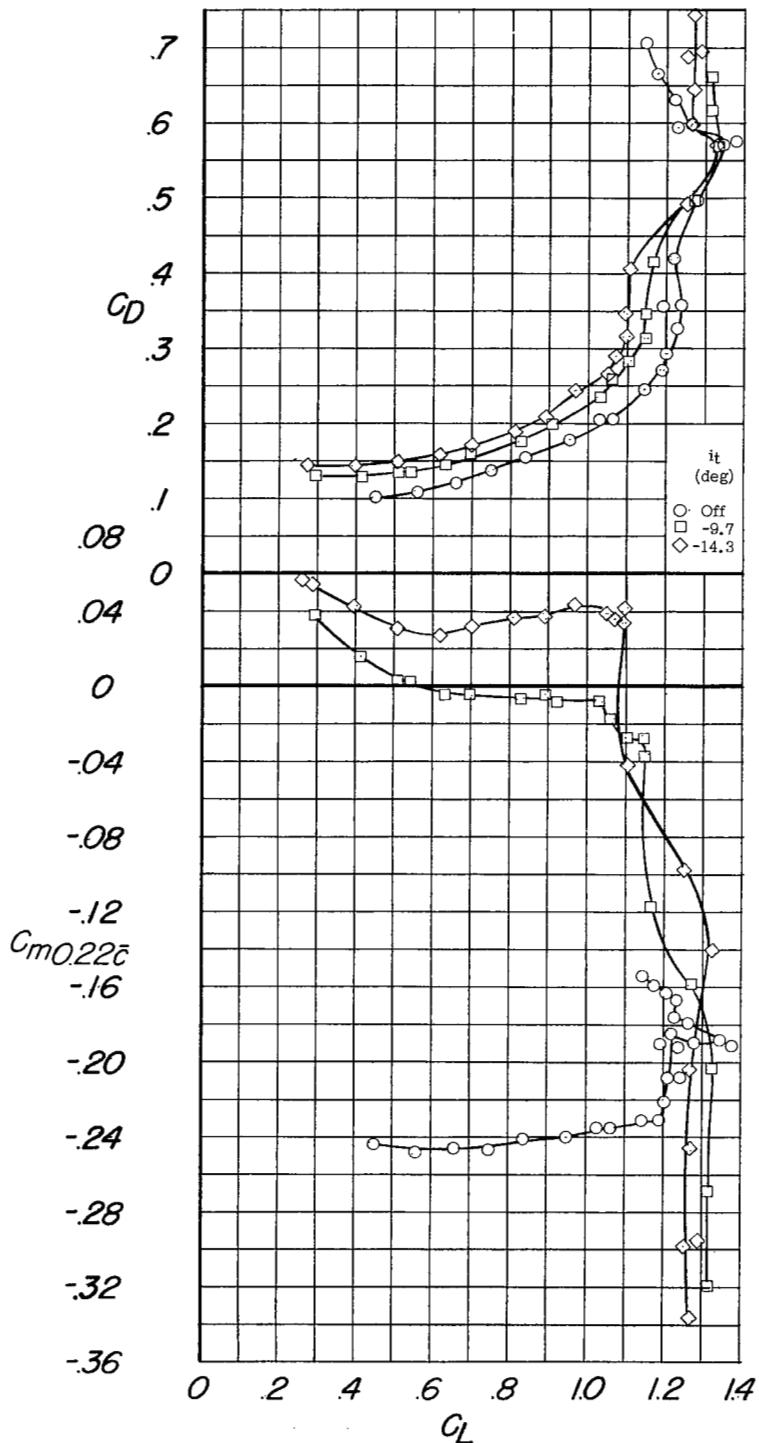
(b) C_D and $C_{m0.22\bar{c}}$ against C_L .

Figure 15.- Concluded.

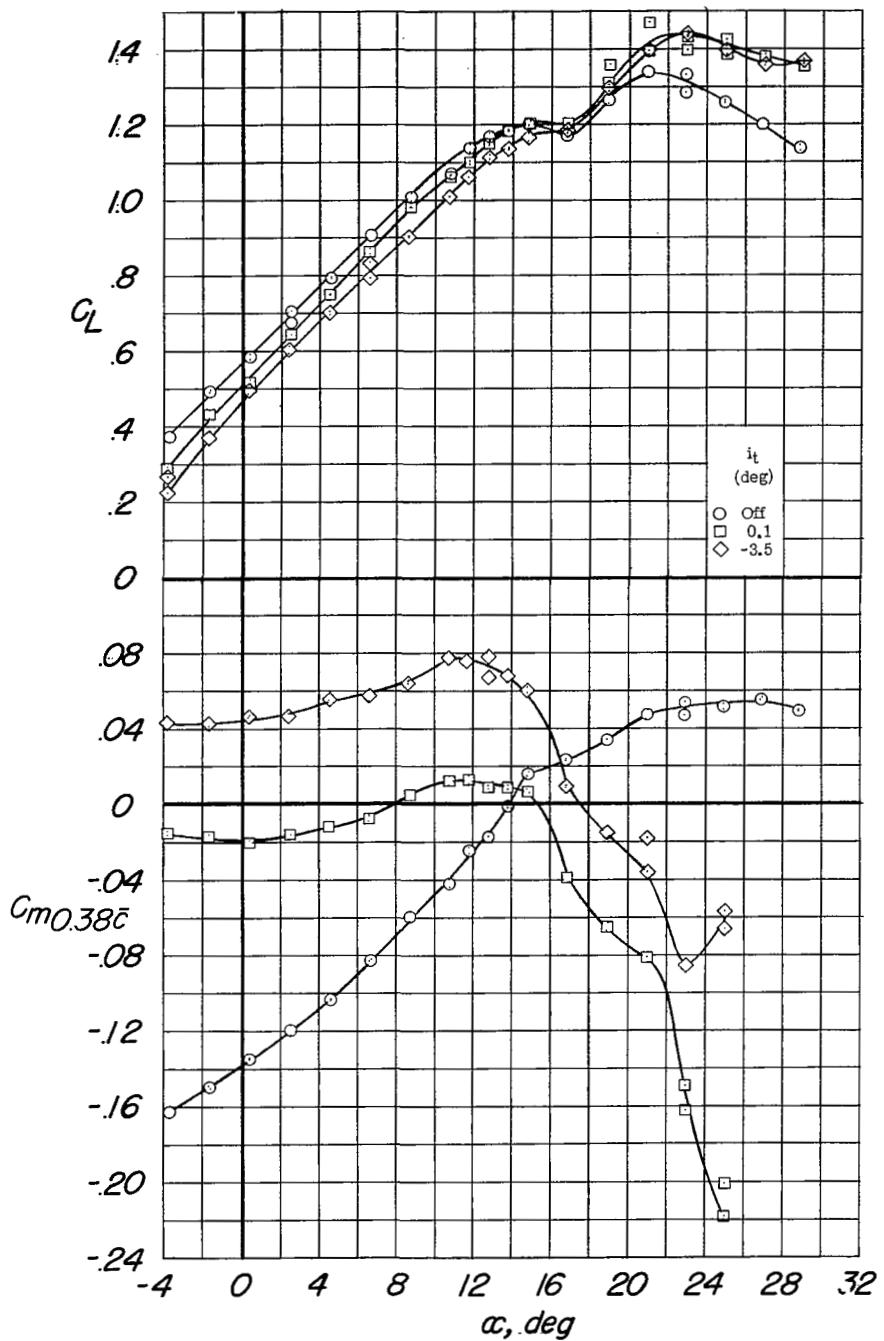
(a) C_L and $C_{m0.38\bar{c}}$ against α .

Figure 16.- Longitudinal characteristics of the model with 80-percent-span trailing-edge flaps deflected 40° and the leading-edge flaps drooped 30° . Configuration: $A + V + I_{SE} + (-0.123)T + 0.80F_{40} + N_{30} + E_0^{450}$; center-of-gravity location, $0.38\bar{c}$.

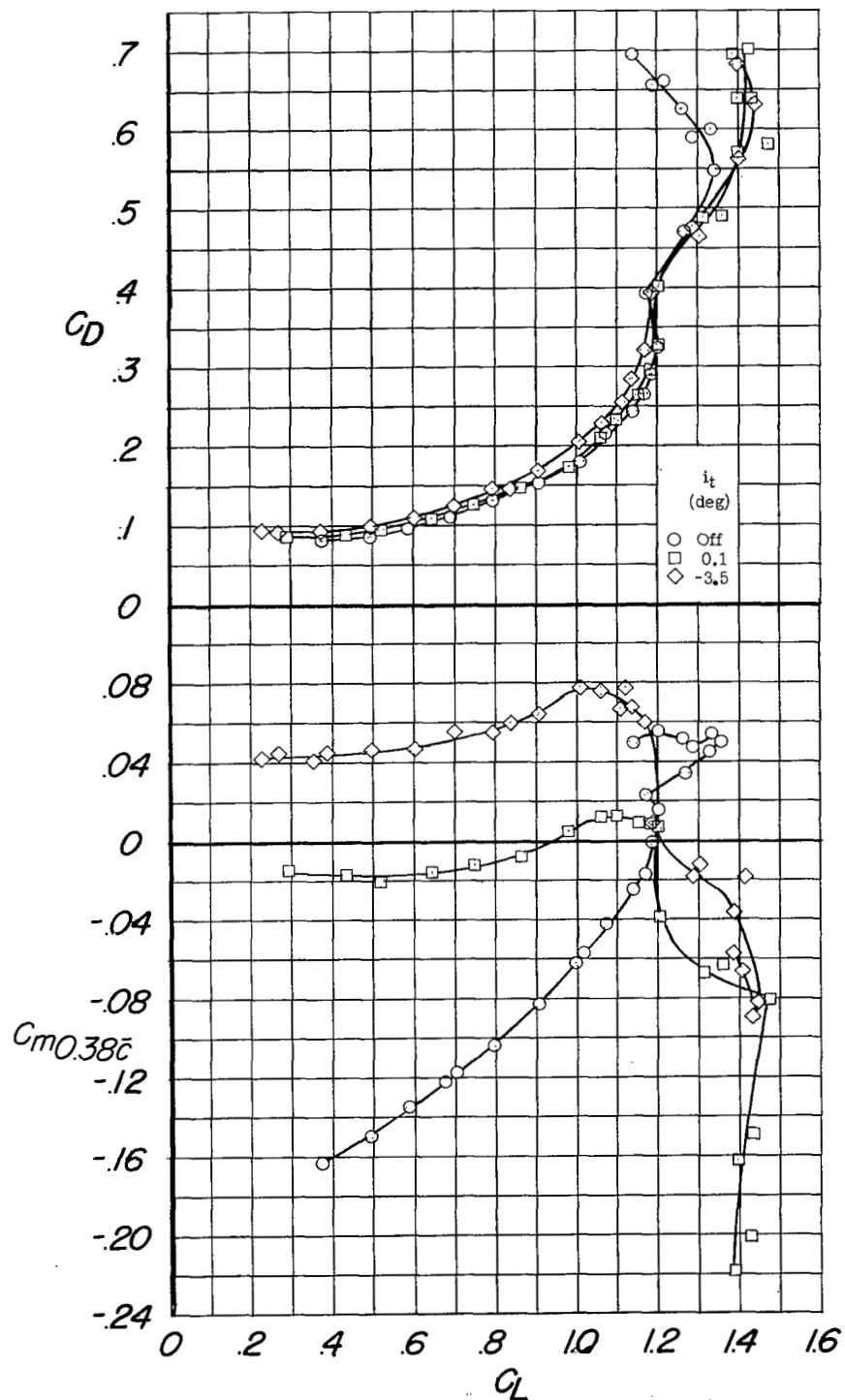
(b) C_D and $C_{m0.38\bar{c}}$ against C_L .

Figure 16.- Concluded.

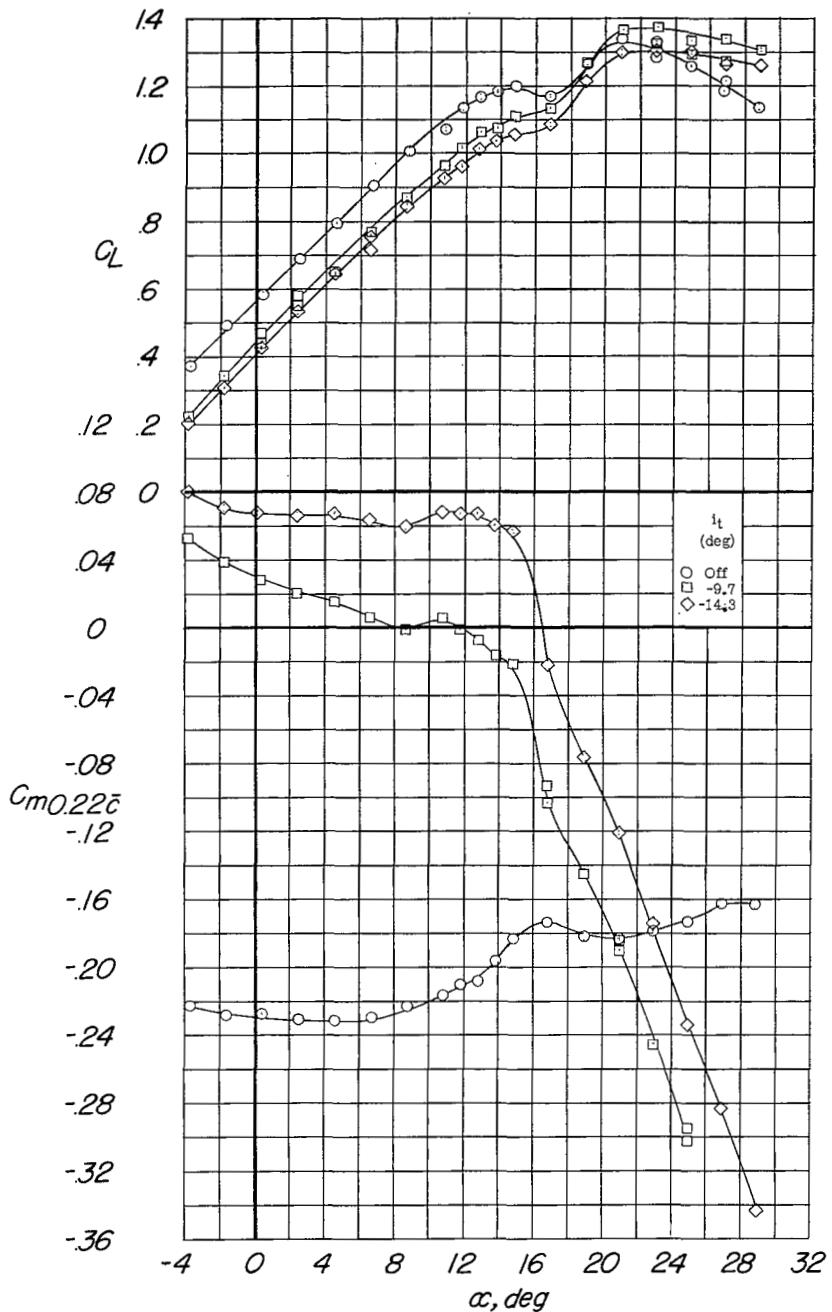
~~CONFIDENTIAL~~(a) C_L and $C_{m,0.22\bar{c}}$ against α .

Figure 17.- Longitudinal characteristics of the model with 80-percent-span trailing-edge flaps deflected 40° and the leading-edge flaps drooped 30° . Configuration: A + V + I_{SE} + (-0.123)T + 0.80F₄₀ + N₃₀ + E₀₄₅₀; center-of-gravity location, $0.22\bar{c}$.

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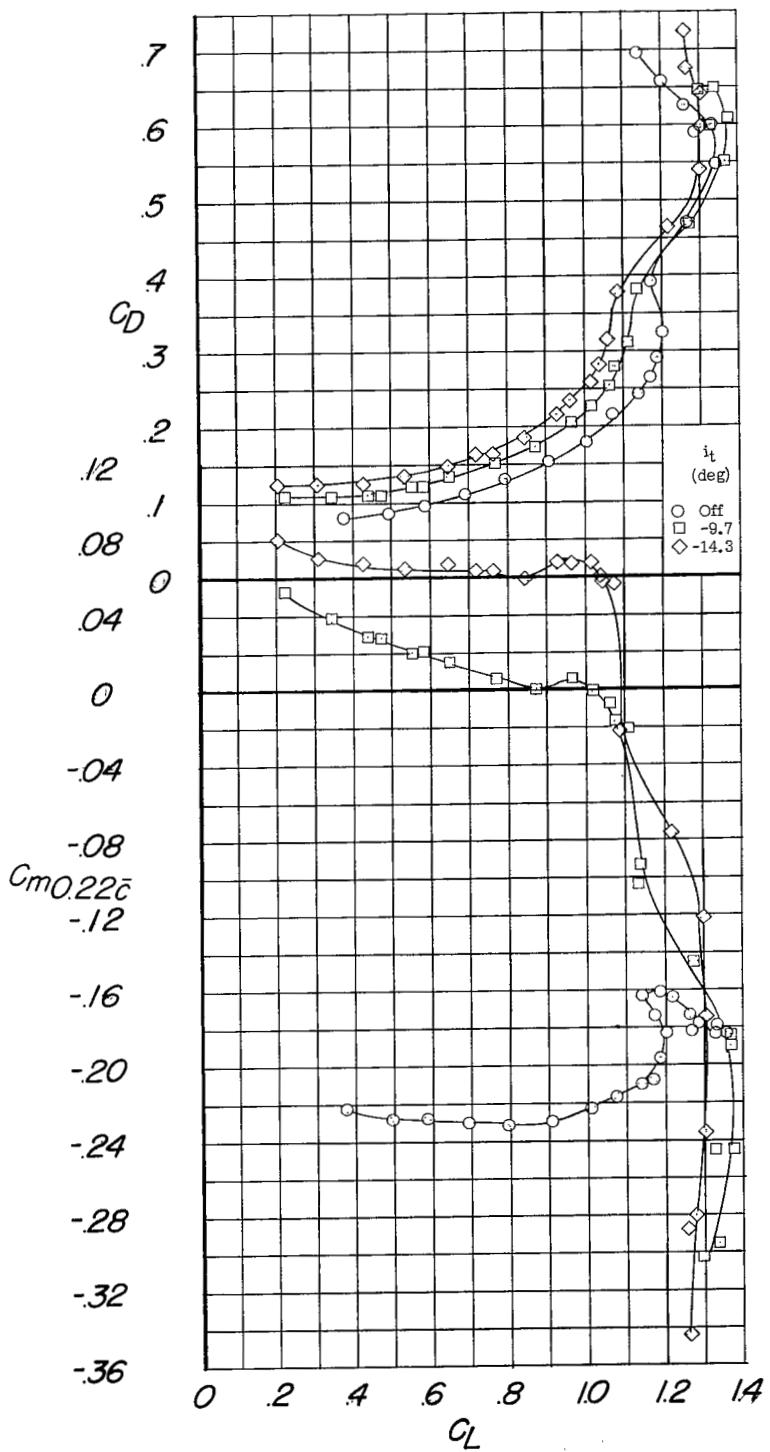
~~CONFIDENTIAL~~(b) C_D and $C_{m0.22\bar{c}}$ against C_L .

Figure 17.- Concluded.

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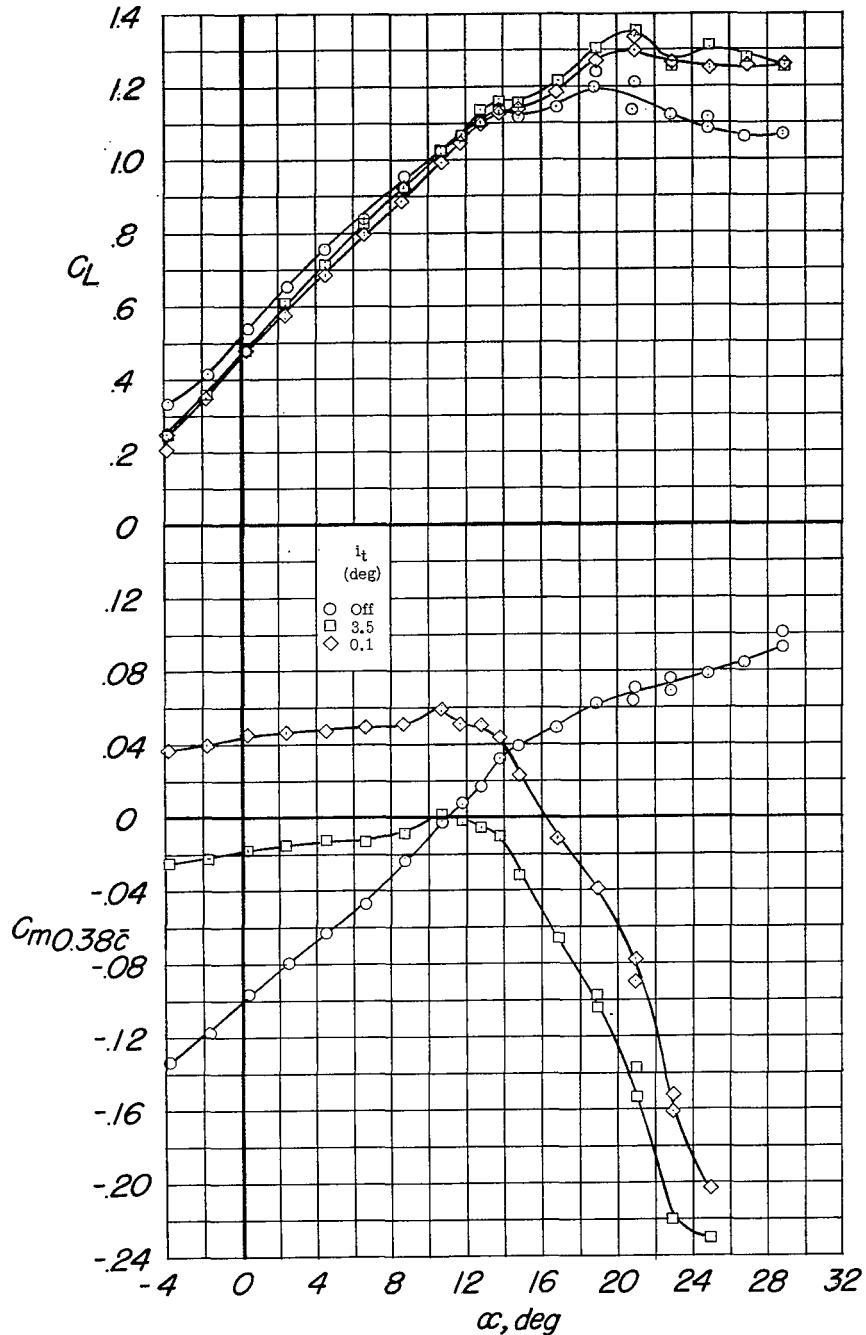
(a) C_L and $C_{m0.38\bar{c}}$ against α .

Figure 18.- Longitudinal characteristics of the model with 70-percent-span trailing-edge flaps deflected 40° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T + 0.70F₄₀ + N₂₀ + E₀450; center-of-gravity location, $0.38\bar{c}$.

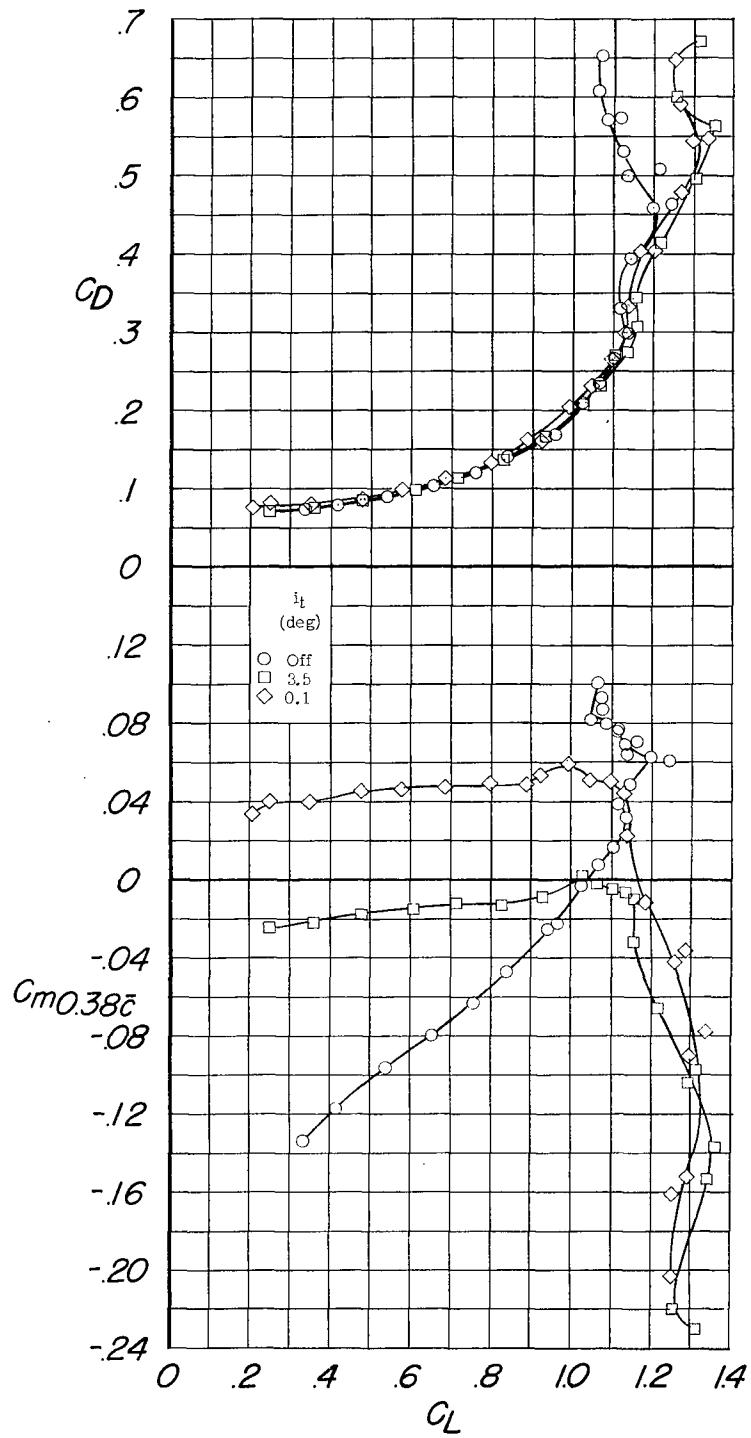
~~CONFIDENTIAL~~(b) C_D and $C_m 0.38\bar{c}$ against C_L .

Figure 18.- Concluded.

~~CONFIDENTIAL~~

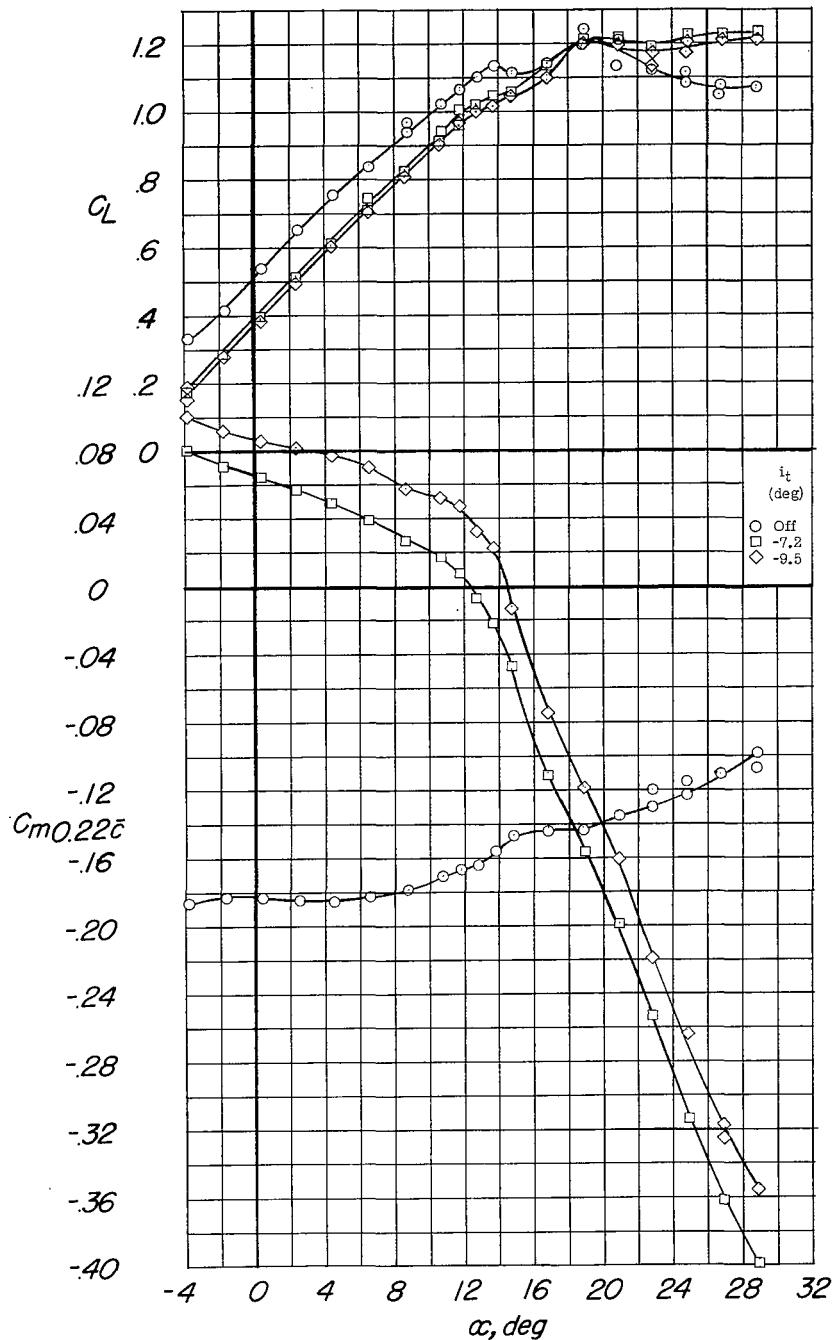
~~CONFIDENTIAL~~(a) C_L and $C_{m,0.22\bar{c}}$ against α .

Figure 19.- Longitudinal characteristics of the model with 70-percent-span trailing-edge flaps deflected 40° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T + 0.70F₄₀ + N₂₀ + E₀⁴⁵⁰; center-of-gravity location, $0.22\bar{c}$.

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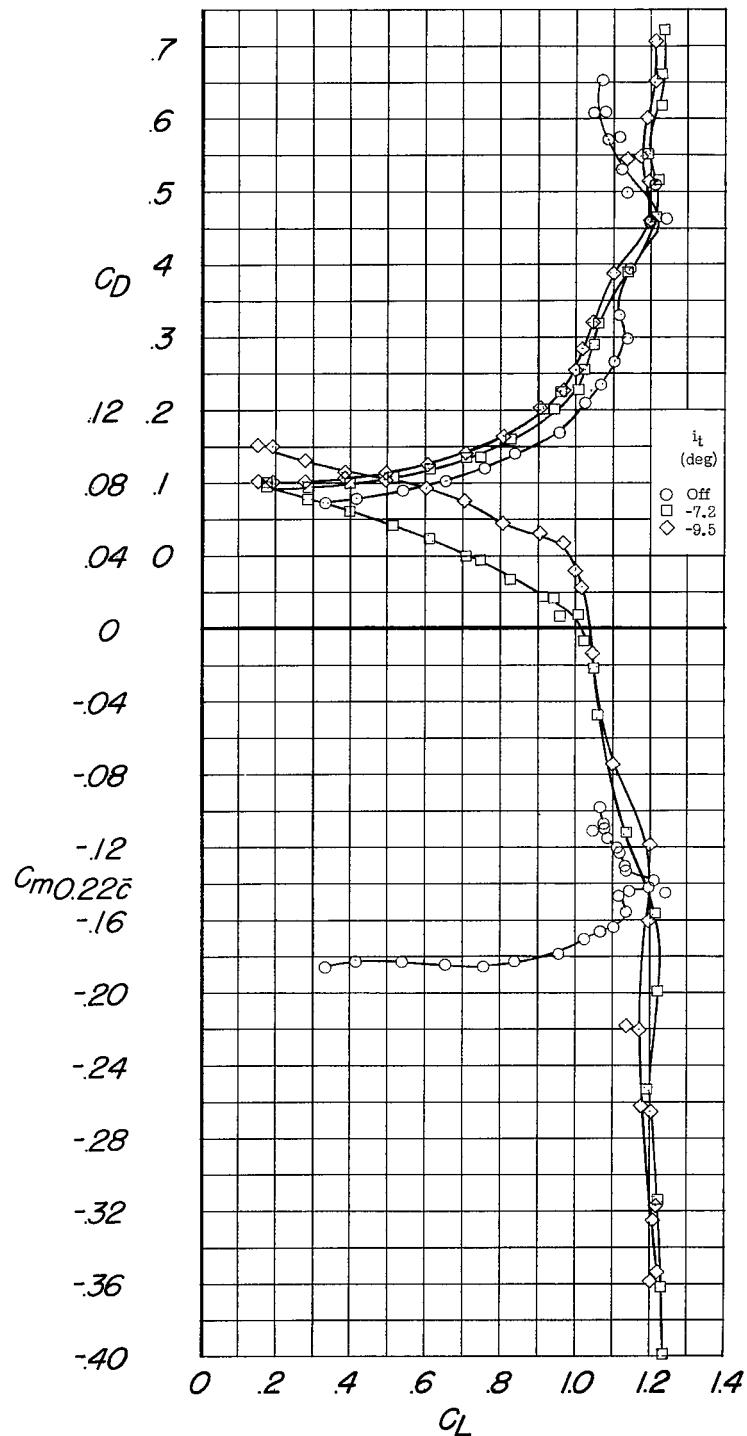
(b) C_D and $C_{m0.22c}$ against C_L .

Figure 19.- Concluded.

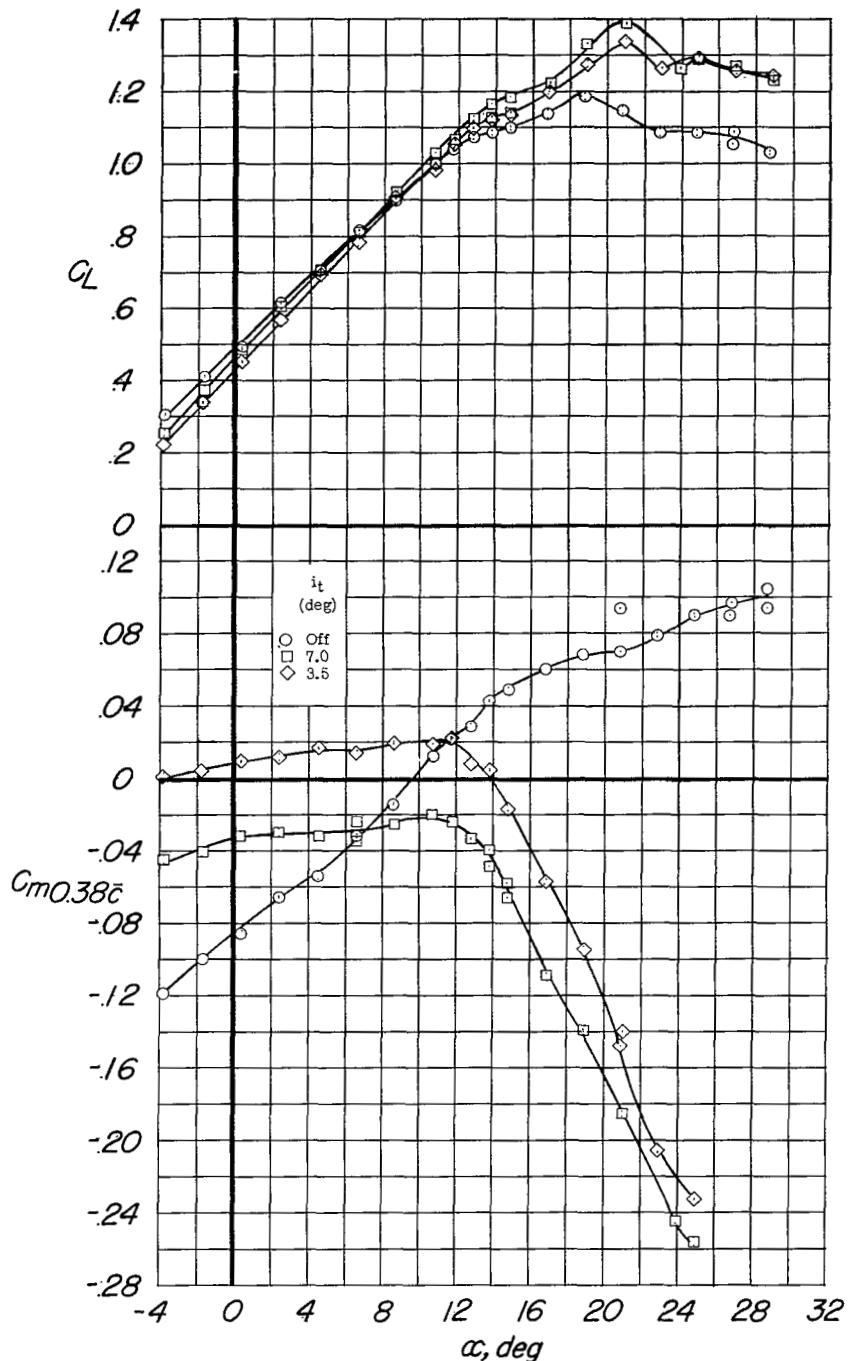
~~CONFIDENTIAL~~(a) C_L and $C_{m0.38\bar{c}}$ against α .

Figure 20.- Longitudinal characteristics of the model with 65-percent-span trailing-edge flaps deflected 40° and the leading-edge flaps drooped 20° . Configuration: $A + V + I_{SE} + (-0.123)T + 0.65F_{40} + N_{20} + E_0^{450}$; center-of-gravity location, $0.38\bar{c}$.

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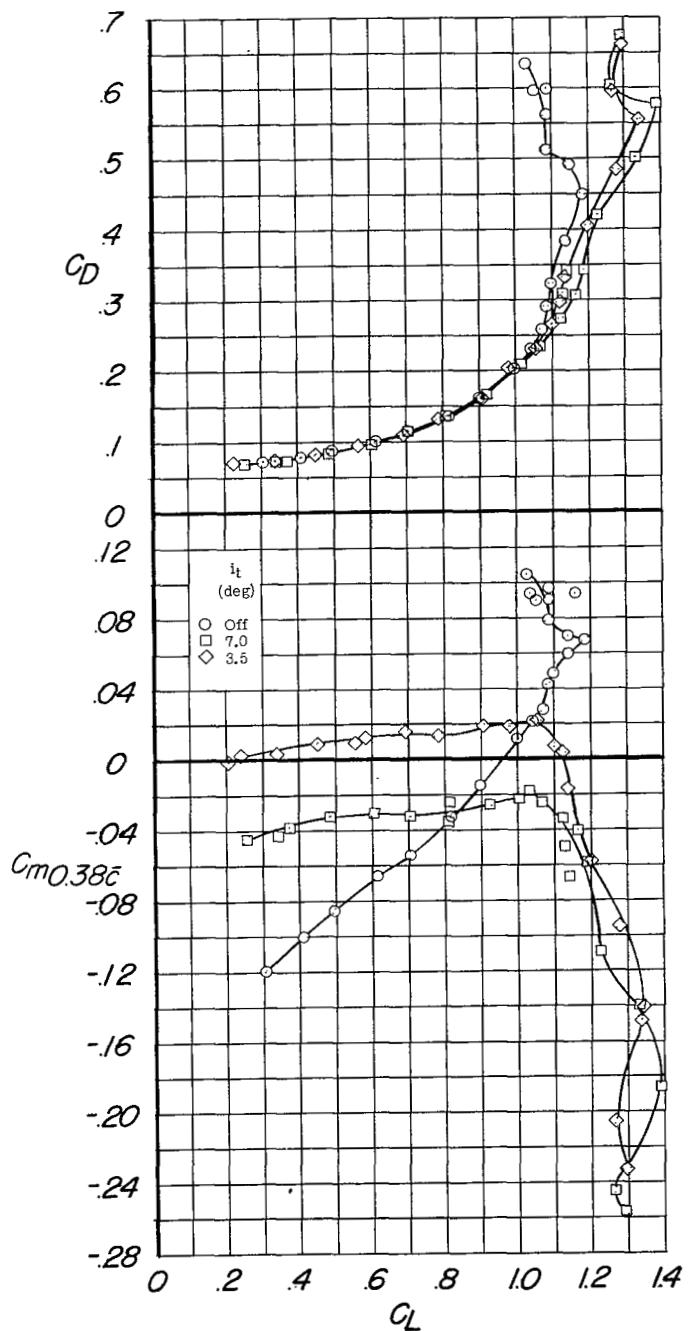
(b) C_D and $C_{m0.38c}$ against C_L .

Figure 20.- Concluded.

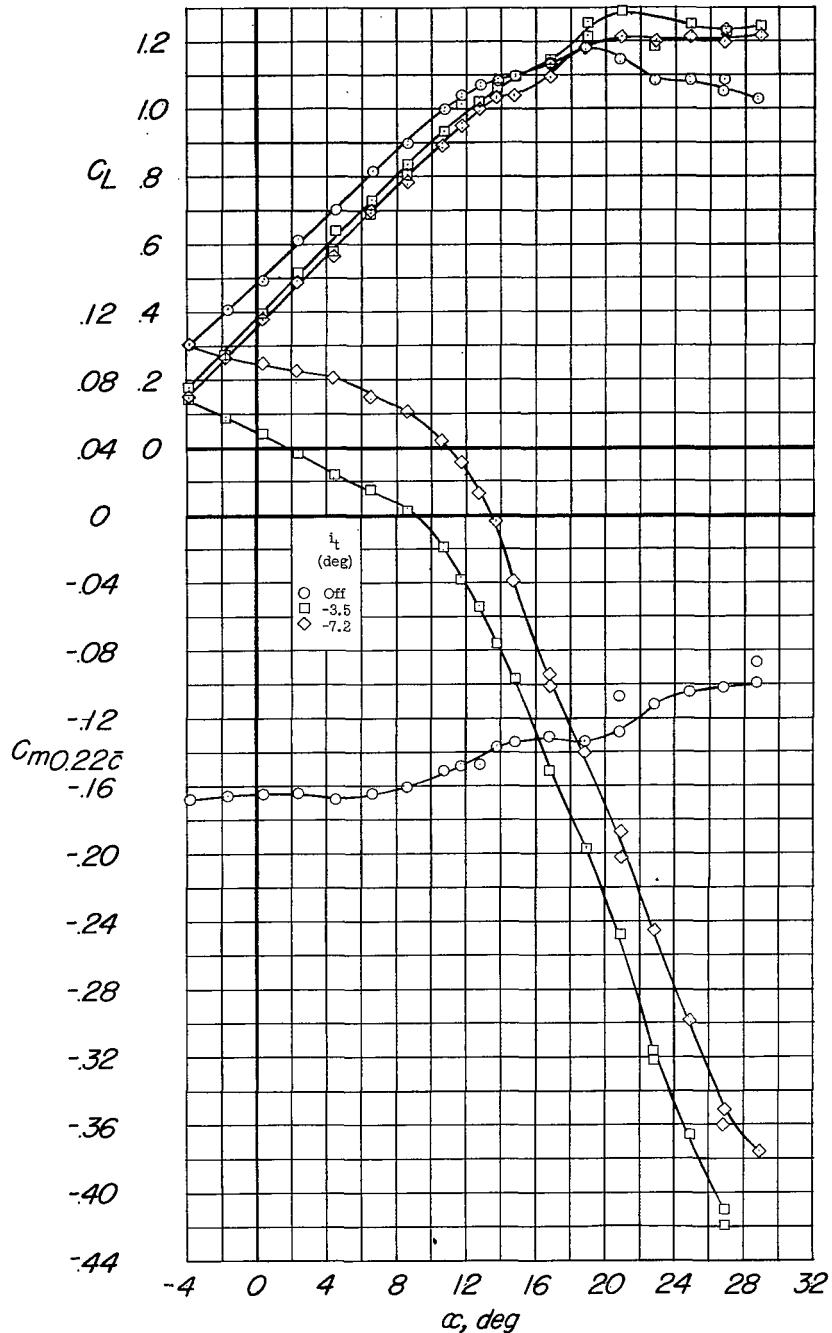
~~CONFIDENTIAL~~(a) C_L and $C_{m,0.22\bar{c}}$ against α .

Figure 21.- Longitudinal characteristics of the model with 65-percent-span trailing-edge flaps deflected 40^0 and the leading-edge flaps drooped 20^0 . Configuration: A + V + I_{SE} + $(-0.123)T + 0.65F_{40} + N_{20} + E_0^{450}$; center-of-gravity location, $0.22\bar{c}$.

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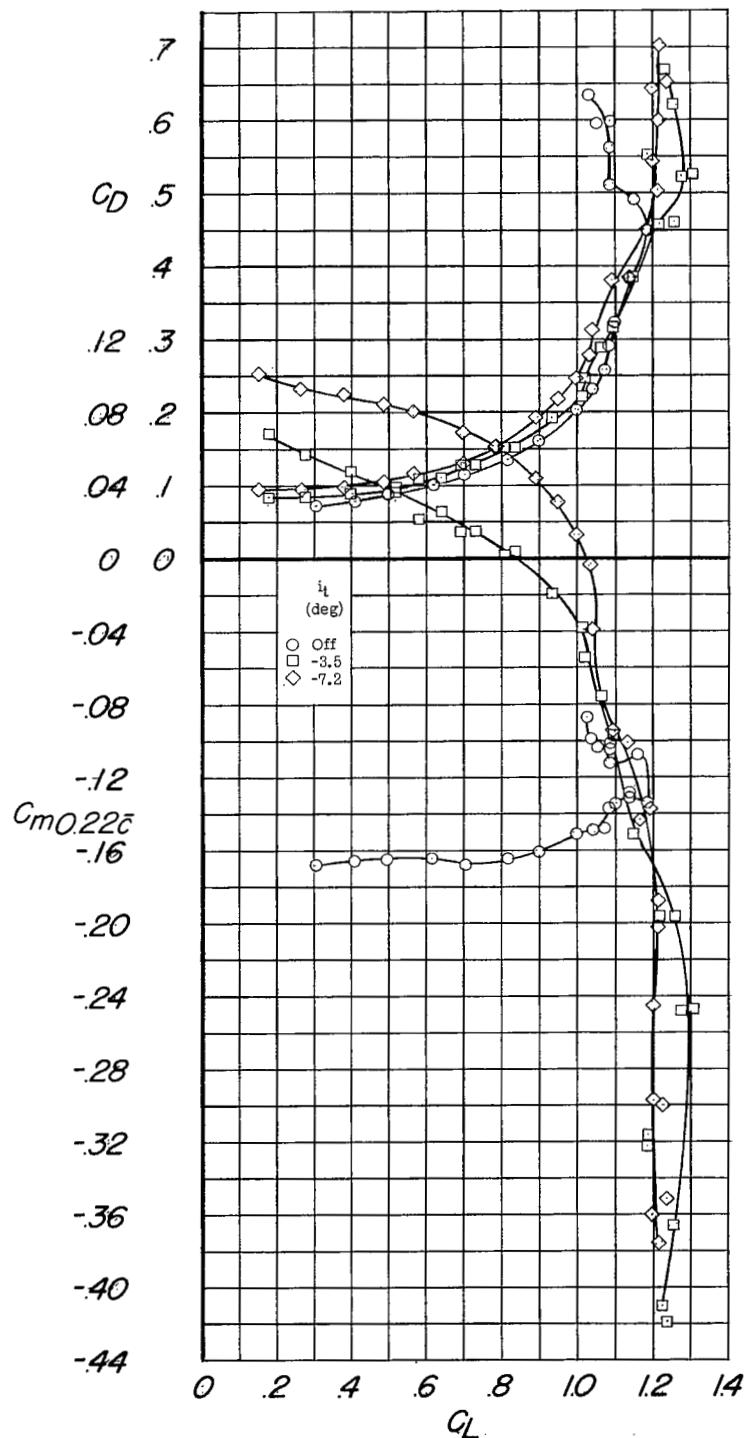
(b) C_D and $C_{m0.22c}$ against C_L .

Figure 21.-- Concluded.

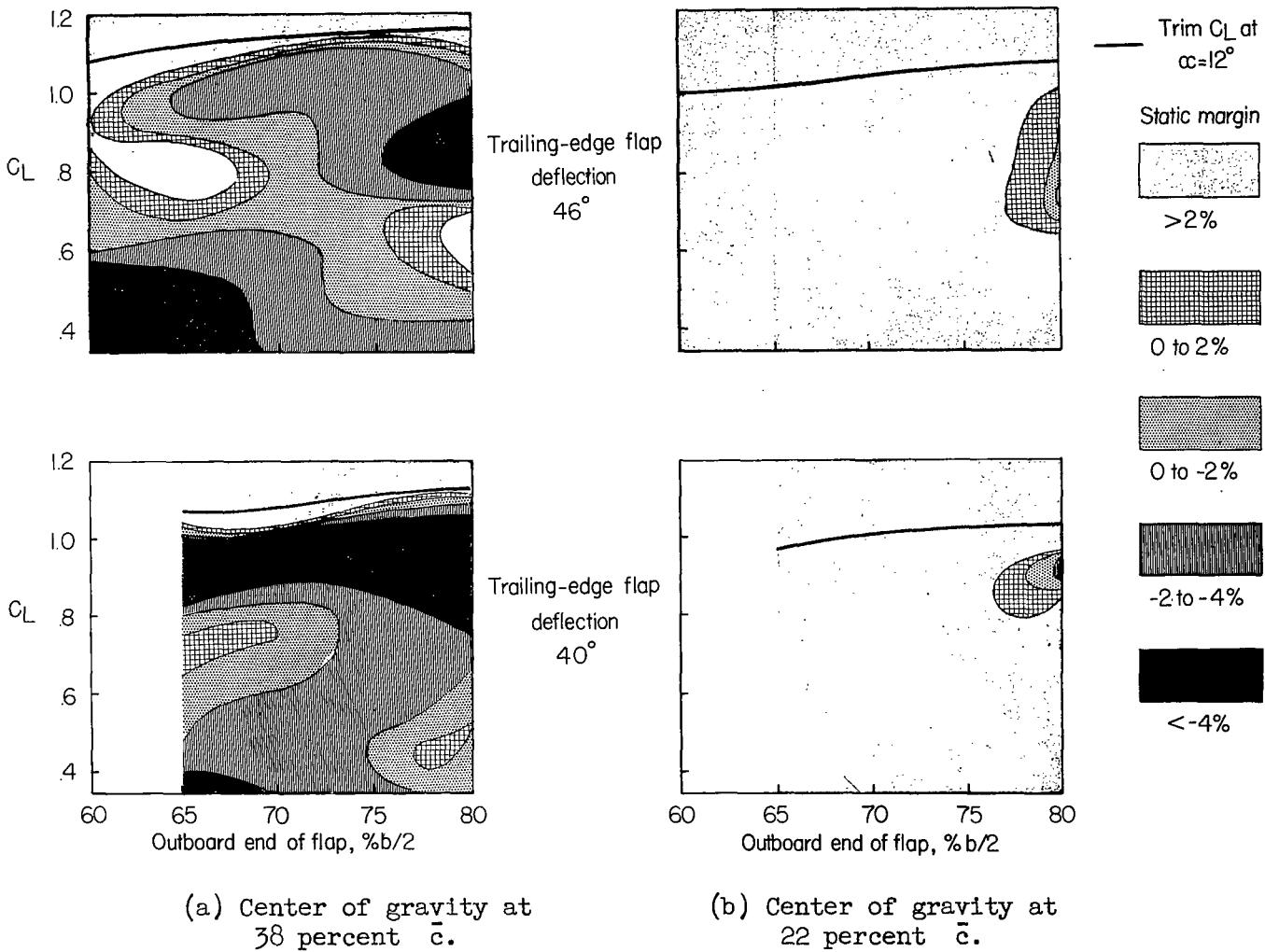


Figure 22.- A summary of the longitudinal stability characteristics of a 1/4-scale model of the F-105 airplane. Configuration: A + V + I_{SE} + F + N + -0.123T.

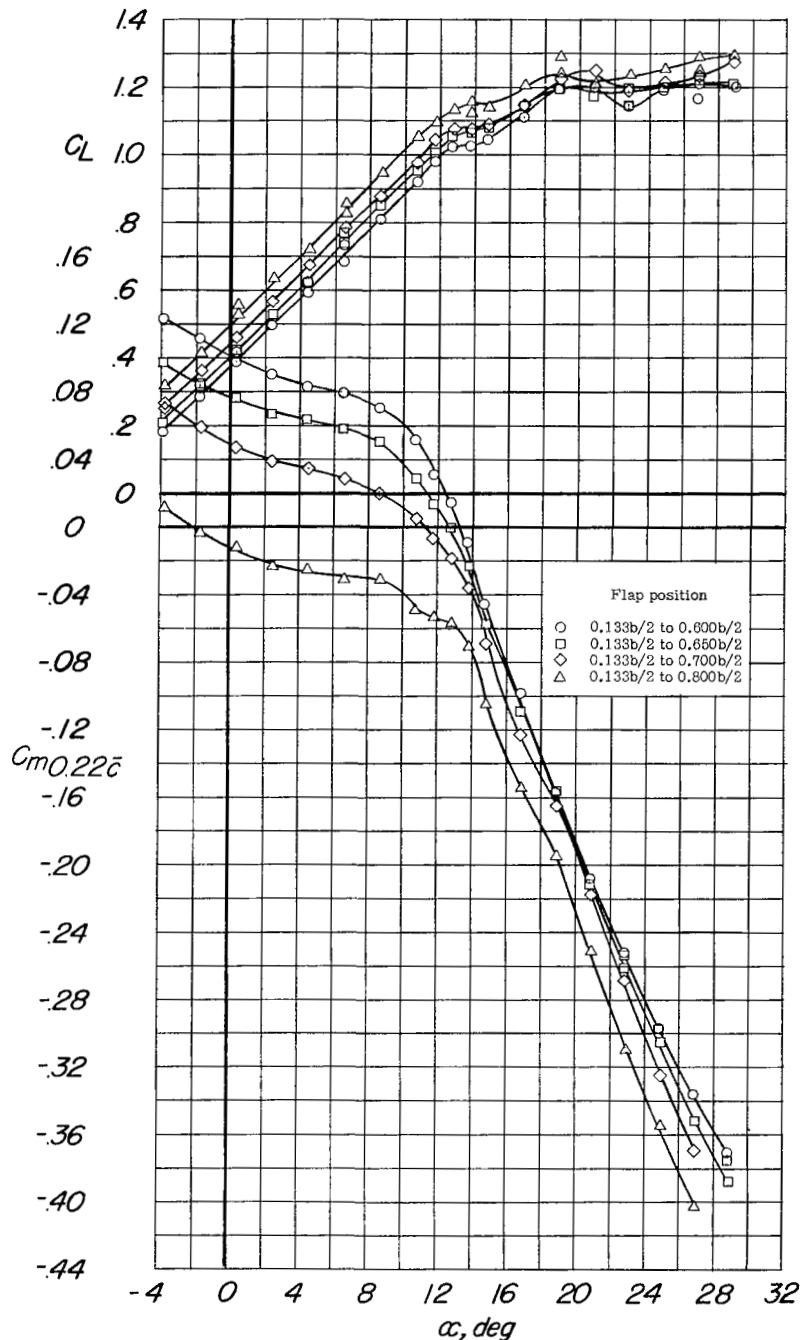
~~CONFIDENTIAL~~(a) C_L and $C_{m,0.22\bar{c}}$ against α .

Figure 23.- Longitudinal characteristics of the model with various span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 20° . Configuration: A + V + I_{SE} + (-0.123)T_{-7.3} + F₄₆ + N₂₀ + E₀⁴⁵⁰; center-of-gravity location, $0.22\bar{c}$.

~~CONFIDENTIAL~~

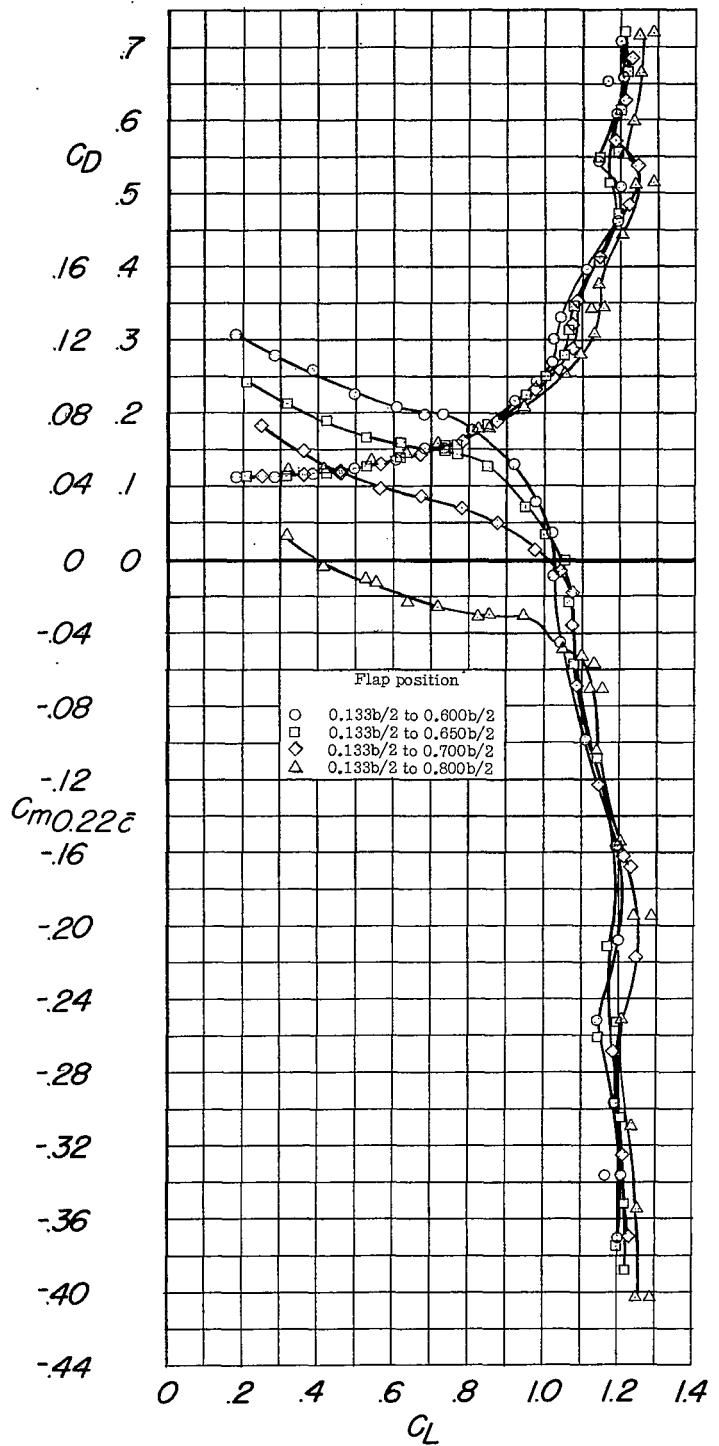
~~CONFIDENTIAL~~(b) C_D and $C_{m0.22\bar{c}}$ against C_L .

Figure 23.- Concluded.

~~CONFIDENTIAL~~

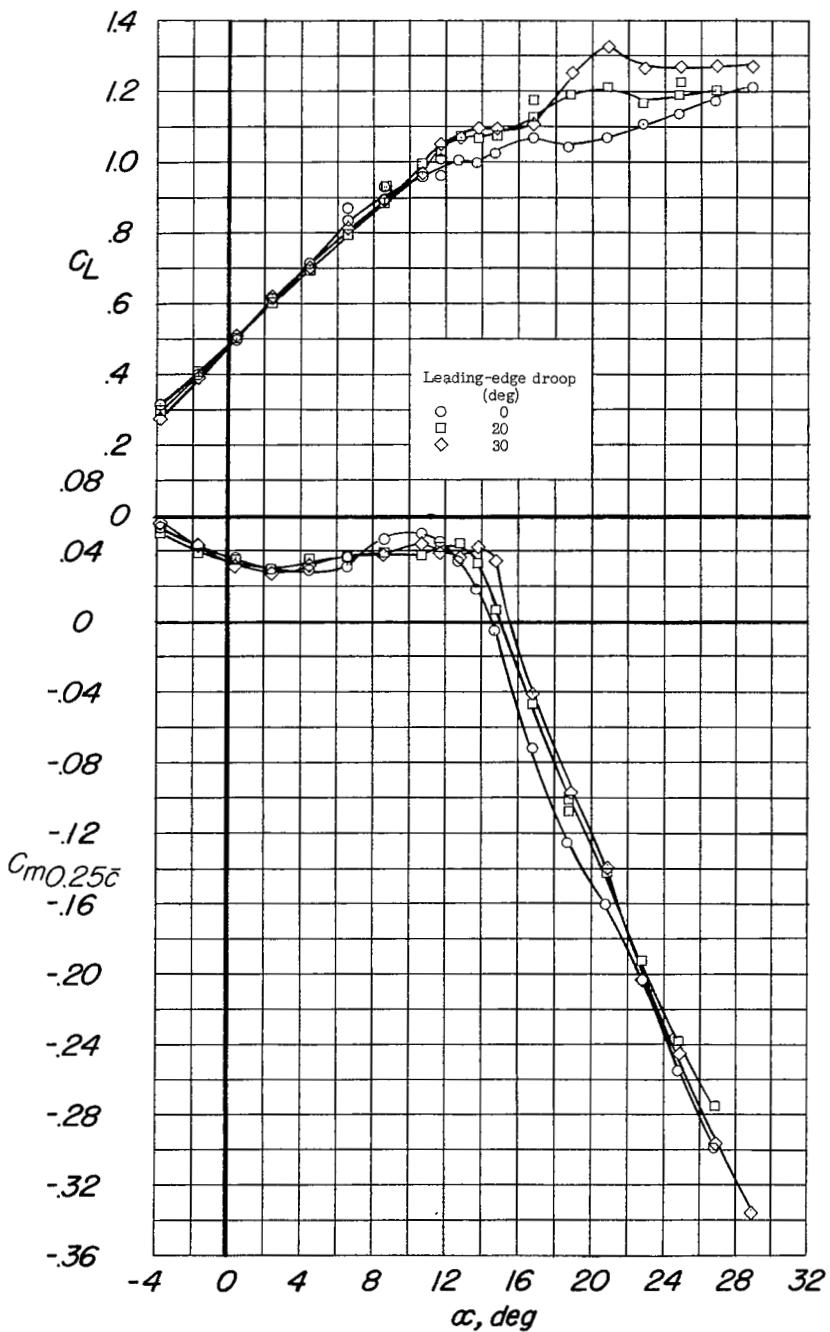
~~CONFIDENTIAL~~(a) C_L and $C_{m0.25c}$ against α .

Figure 24.- Longitudinal characteristics of the model with 80-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped various amounts. Configuration: A + V + I_{SE} + (-0.123)T_{-14.3} + 0.80F₄₆ + N + E₀⁴⁵⁰; center-of-gravity location, $0.25\bar{c}$.

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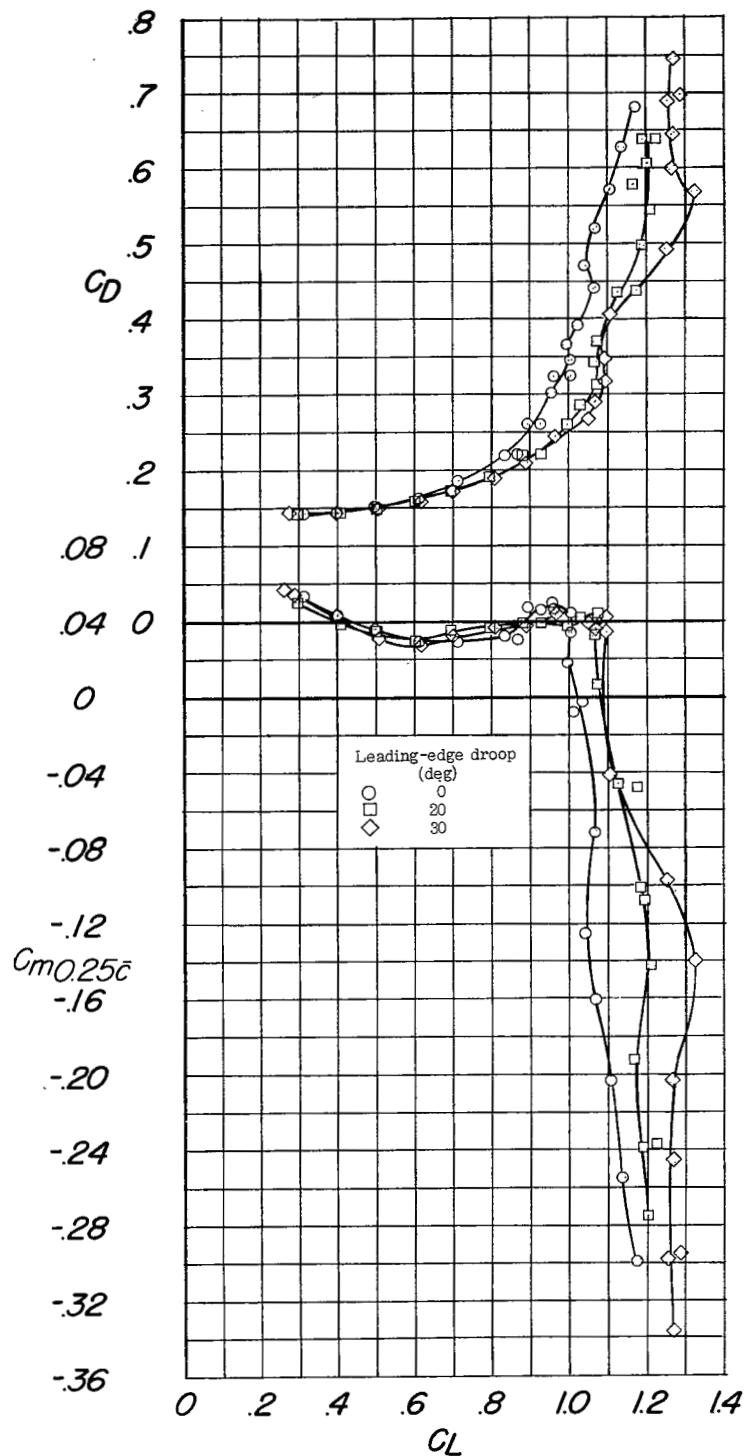
(b) C_D and $C_{m0.25c}$ against C_L .

Figure 24.- Concluded.

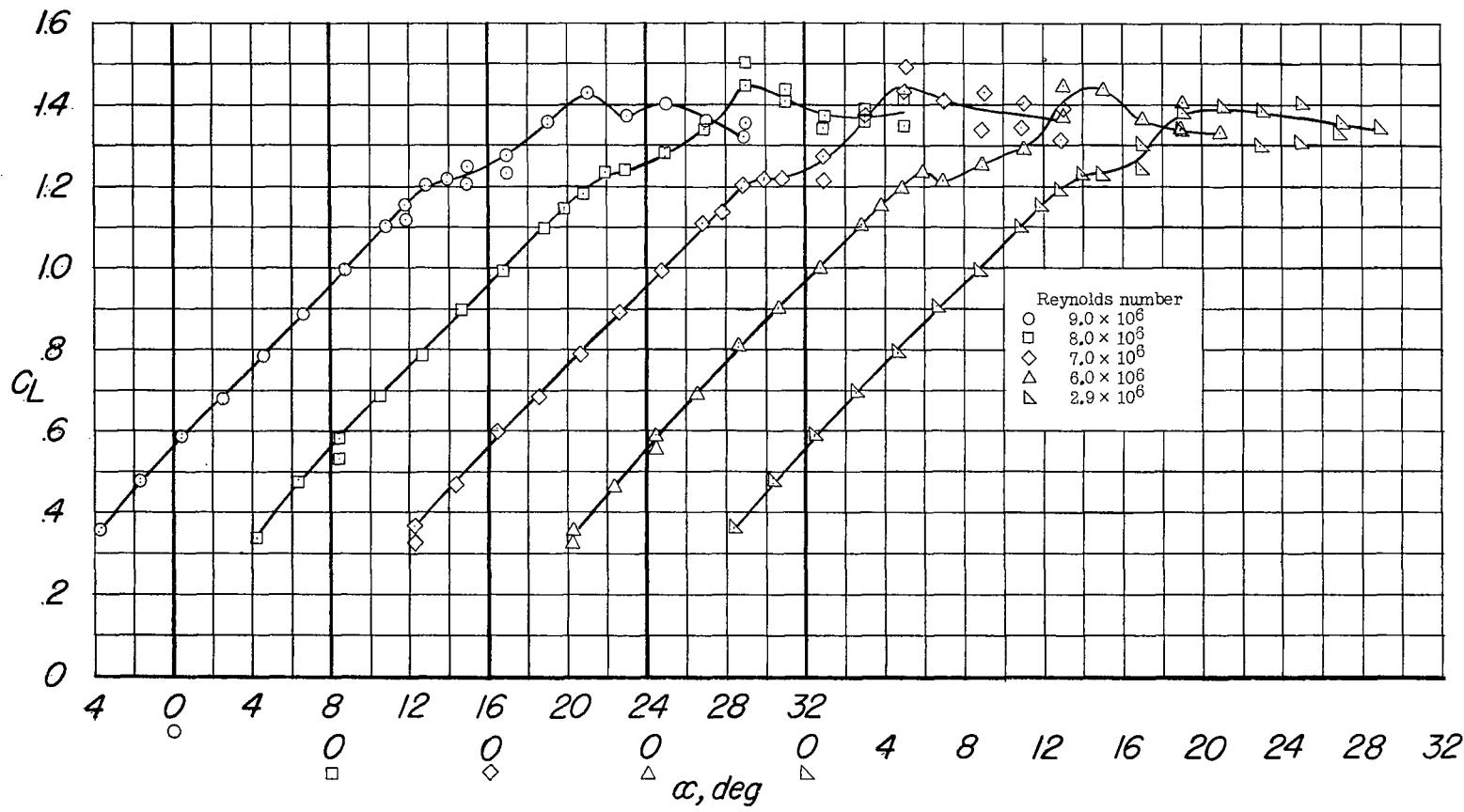
(a) C_L against α .

Figure 25.- Longitudinal characteristics at various Reynolds numbers of the model with 80-percent-span trailing-edge flaps deflected 46° and the leading-edge flaps drooped 30° . Configuration: A + V + ISE + $(-0.123)T_{-0.2} + 0.80F_{46} + N_{30} + E_0^{450}$; center-of-gravity location, $0.25\bar{c}$.

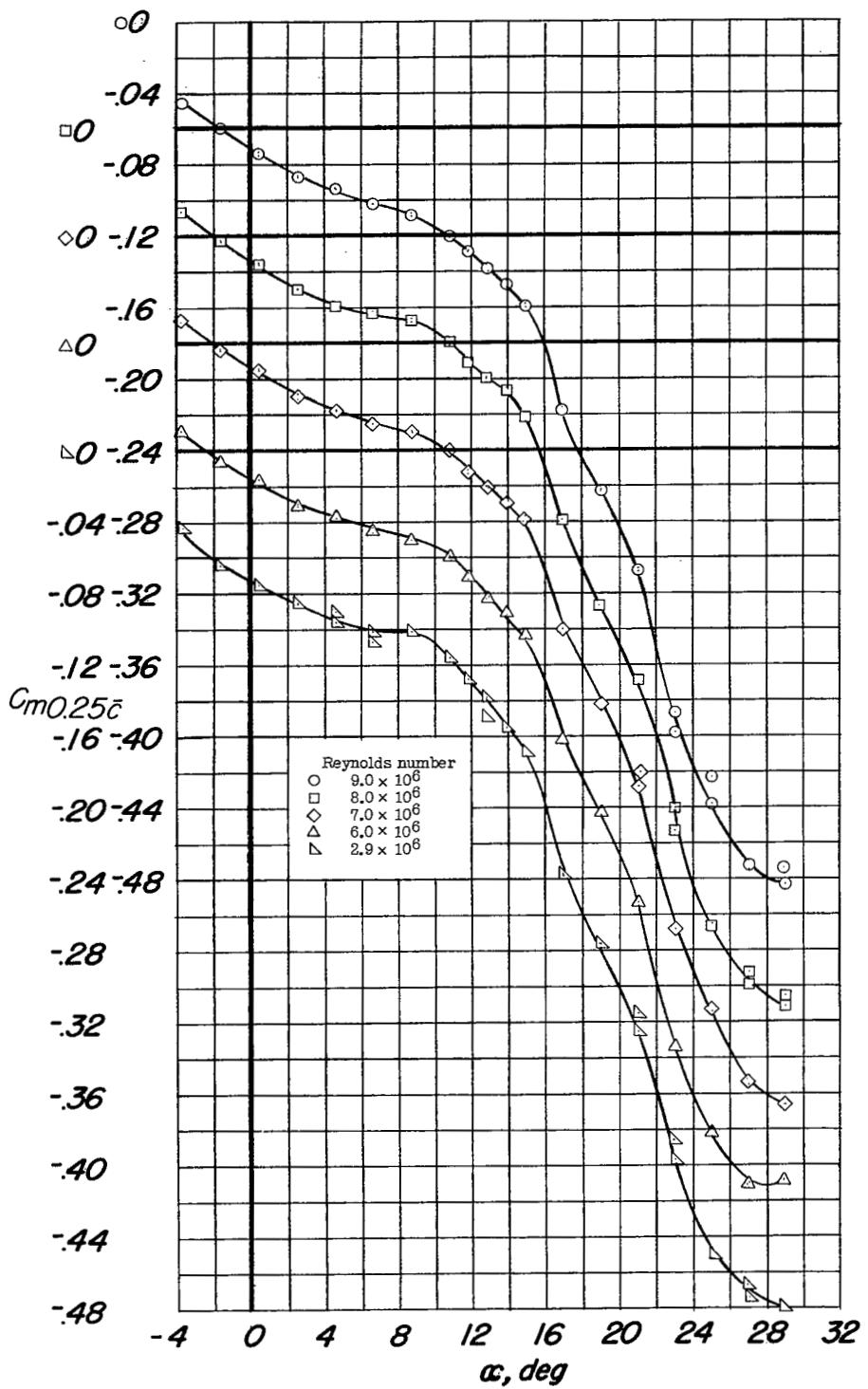
(b) $C_{m0.25\bar{c}}$ against α .

Figure 25.- Continued.

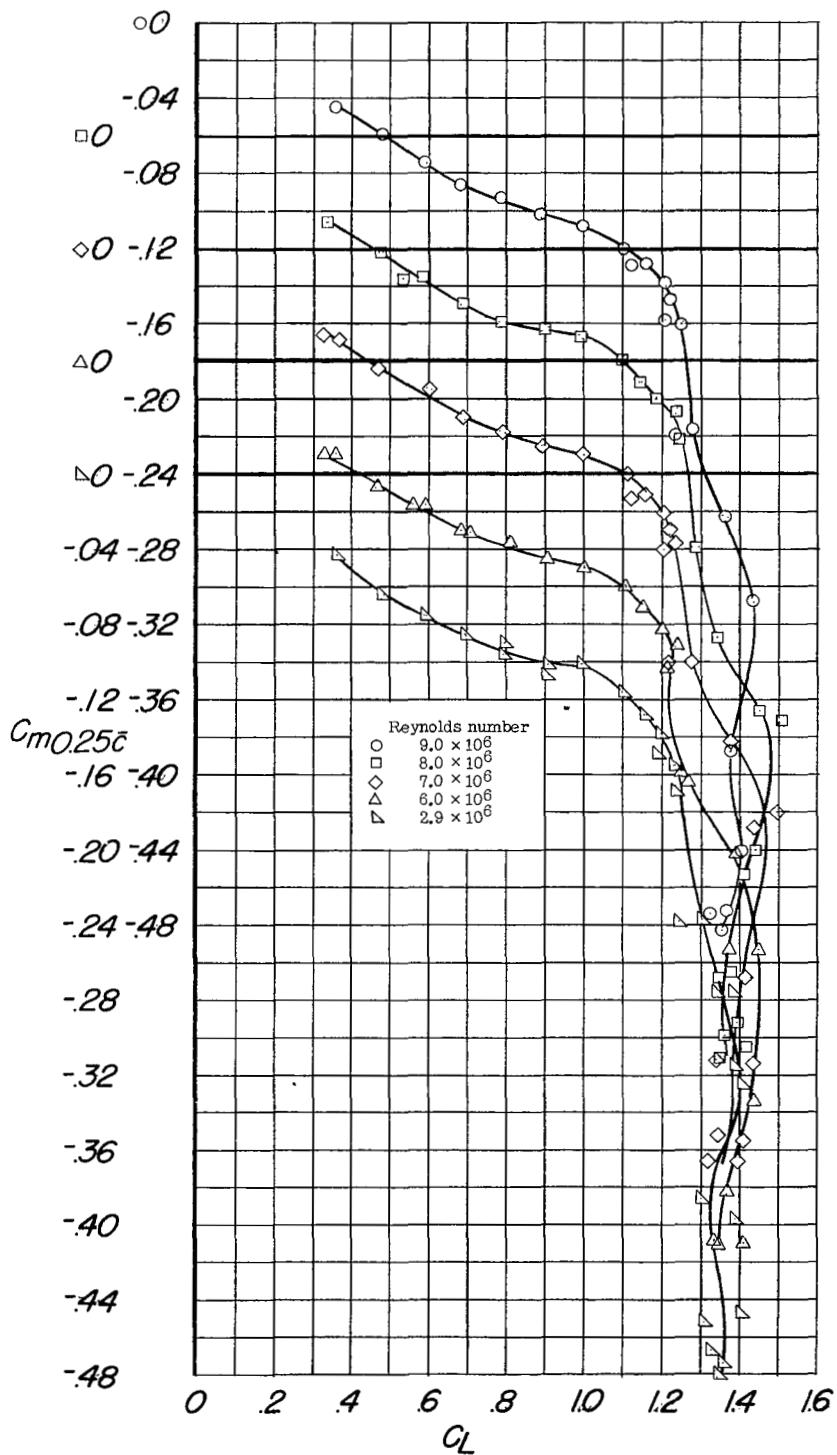
~~CONFIDENTIAL~~(c) $C_{m0.25c}$ against C_L .

Figure 25.- Continued.

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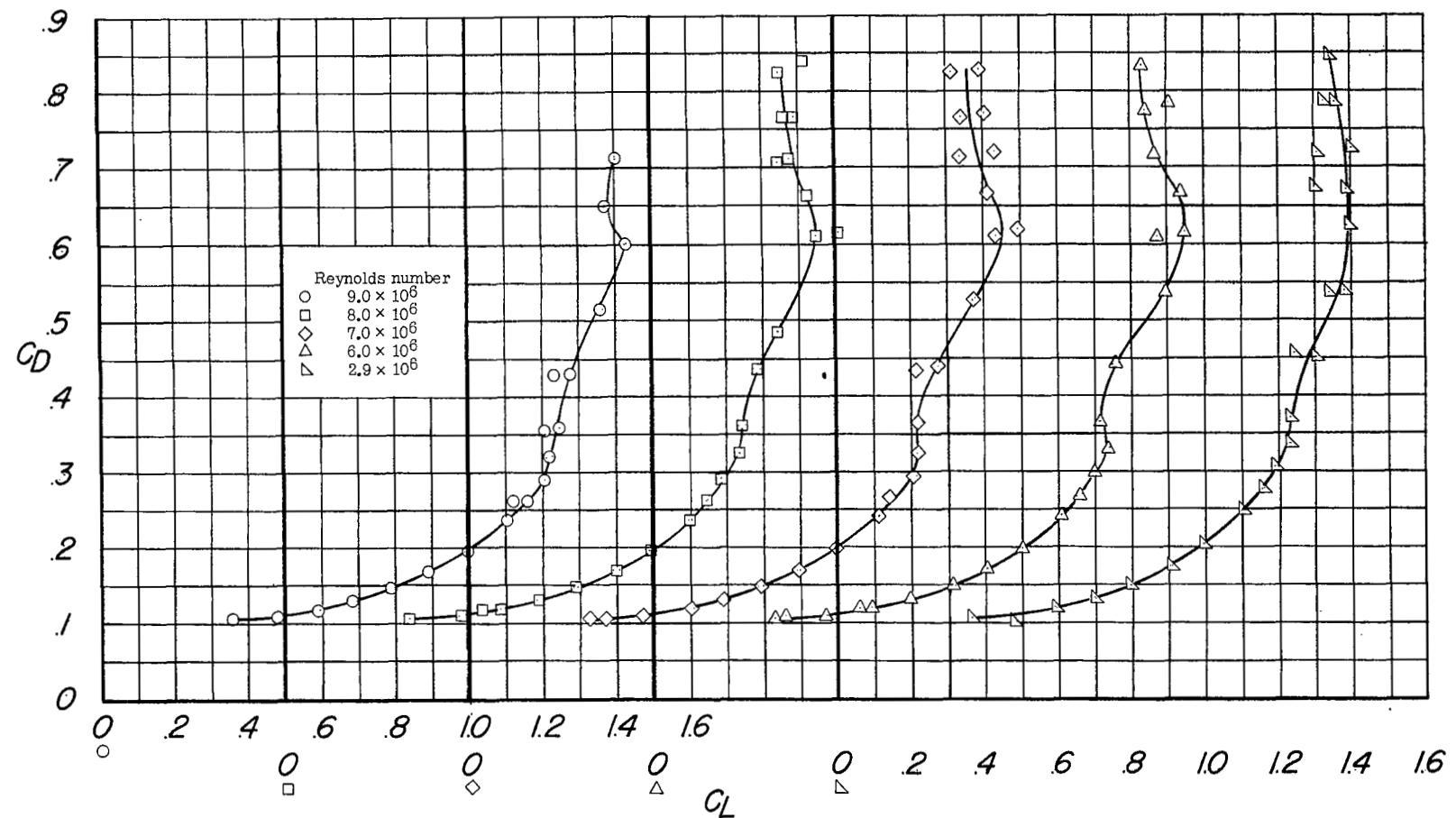
(d) C_D against C_L .

Figure 25.- Concluded.

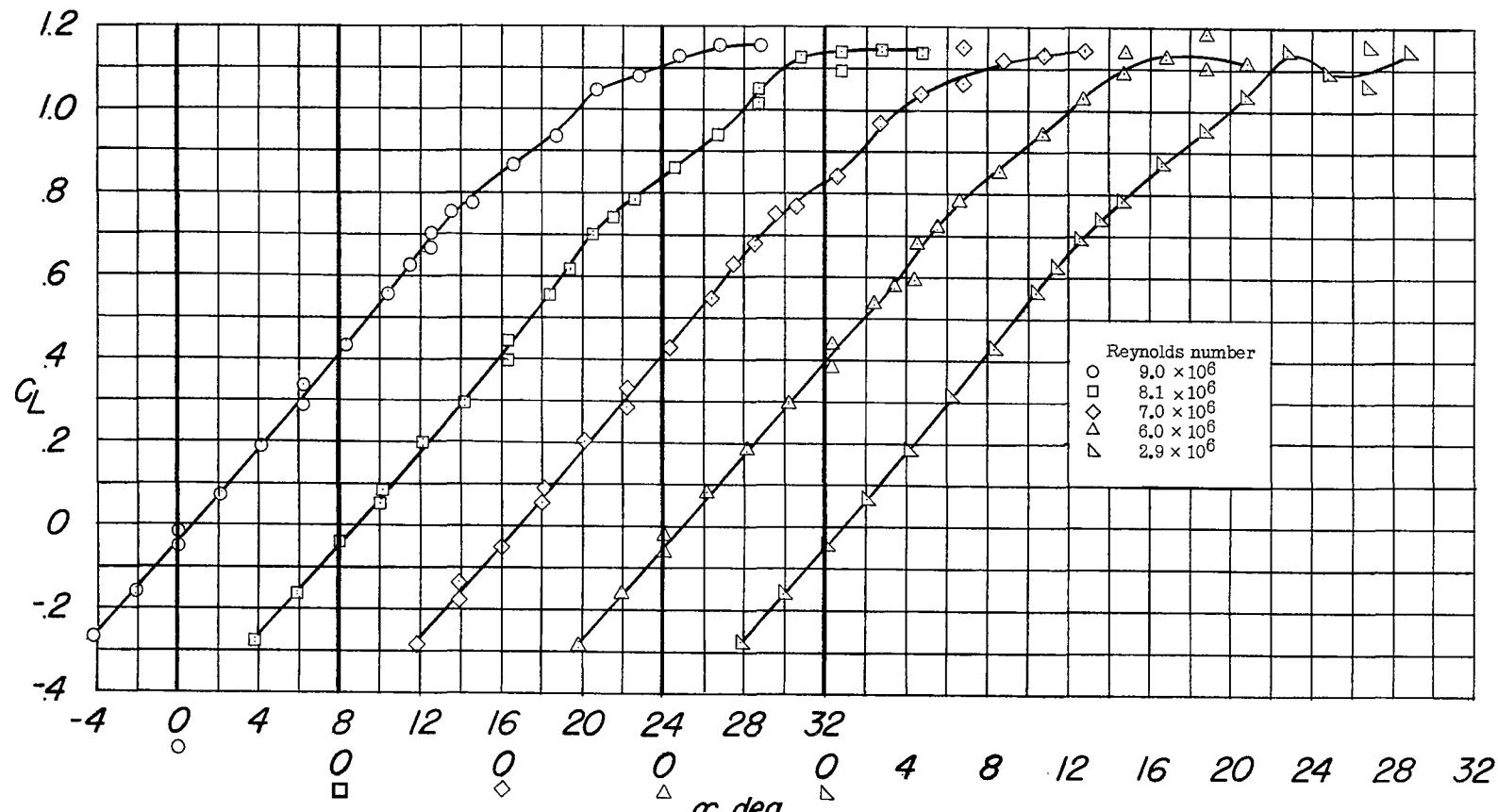
(a) C_L against α .

Figure 26.- Longitudinal characteristics at various Reynolds numbers of the model with the leading-edge flaps drooped 7.5° . Configuration: A + V + ISE + $(-0.123)T_{-3.5}$ + N_{7.5}; center-of-gravity location, $0.25\bar{c}$.

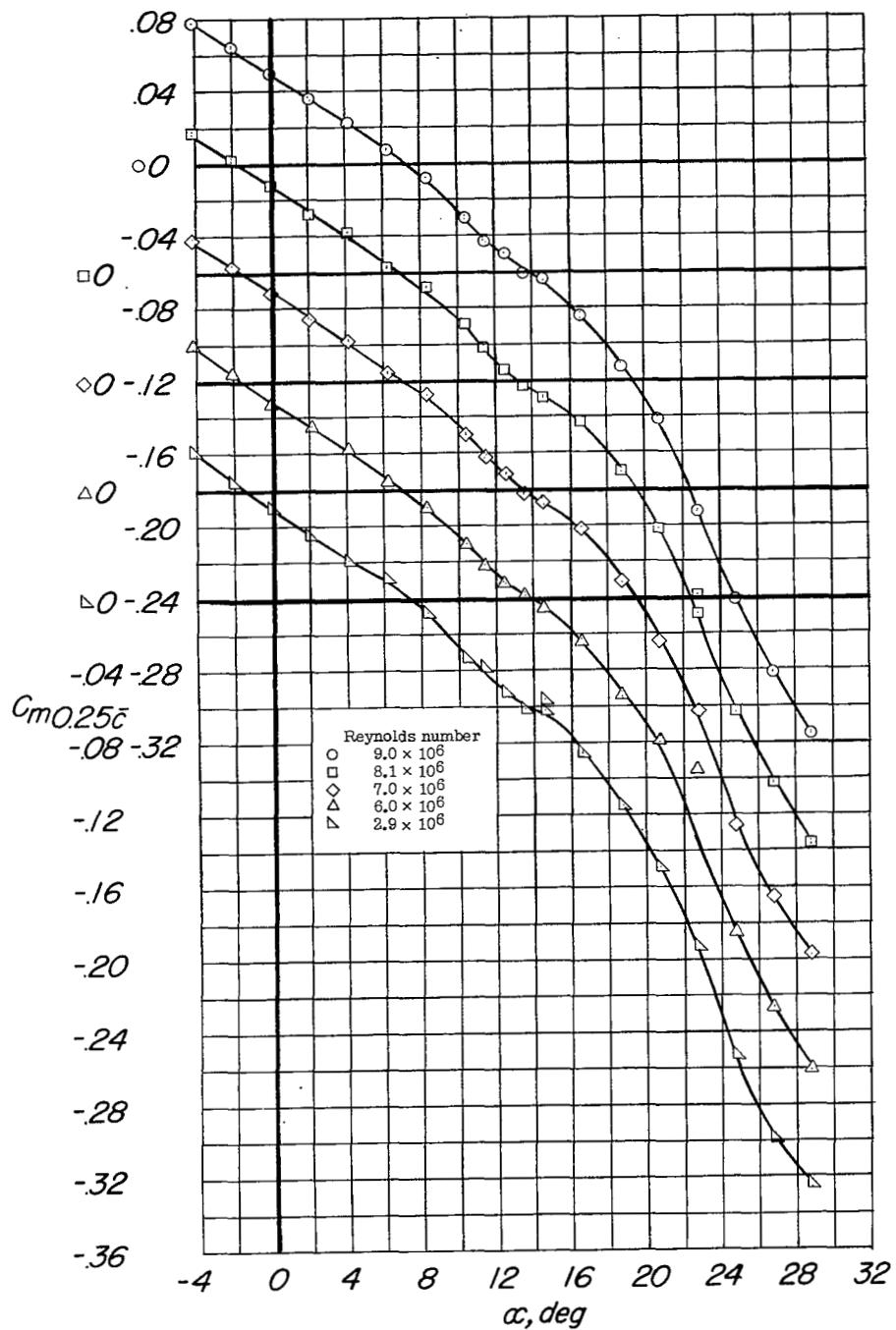
(b) $C_{m0.25\bar{c}}$ against α .

Figure 26.- Continued.

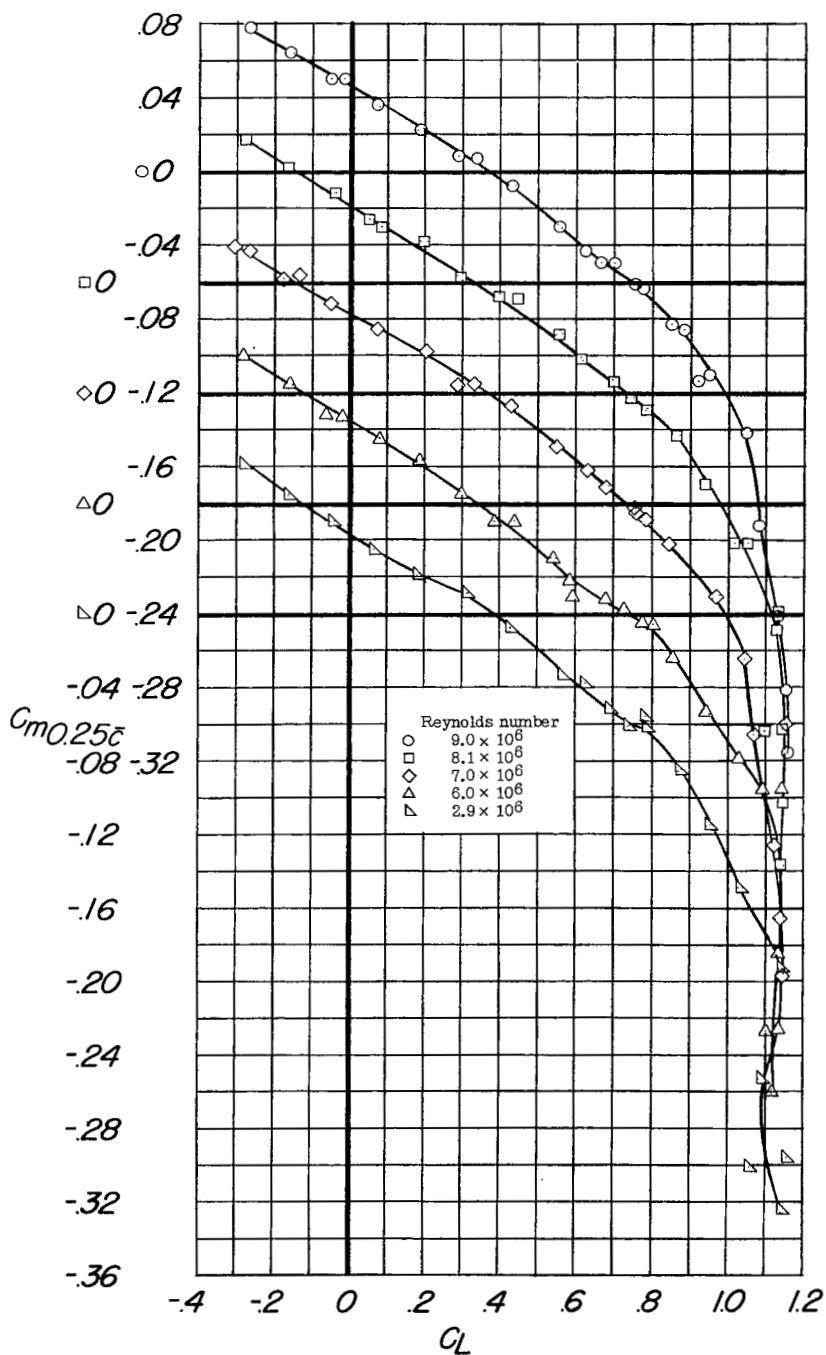
(c) $C_{m0.25c}$ against C_L .

Figure 26.- Continued.

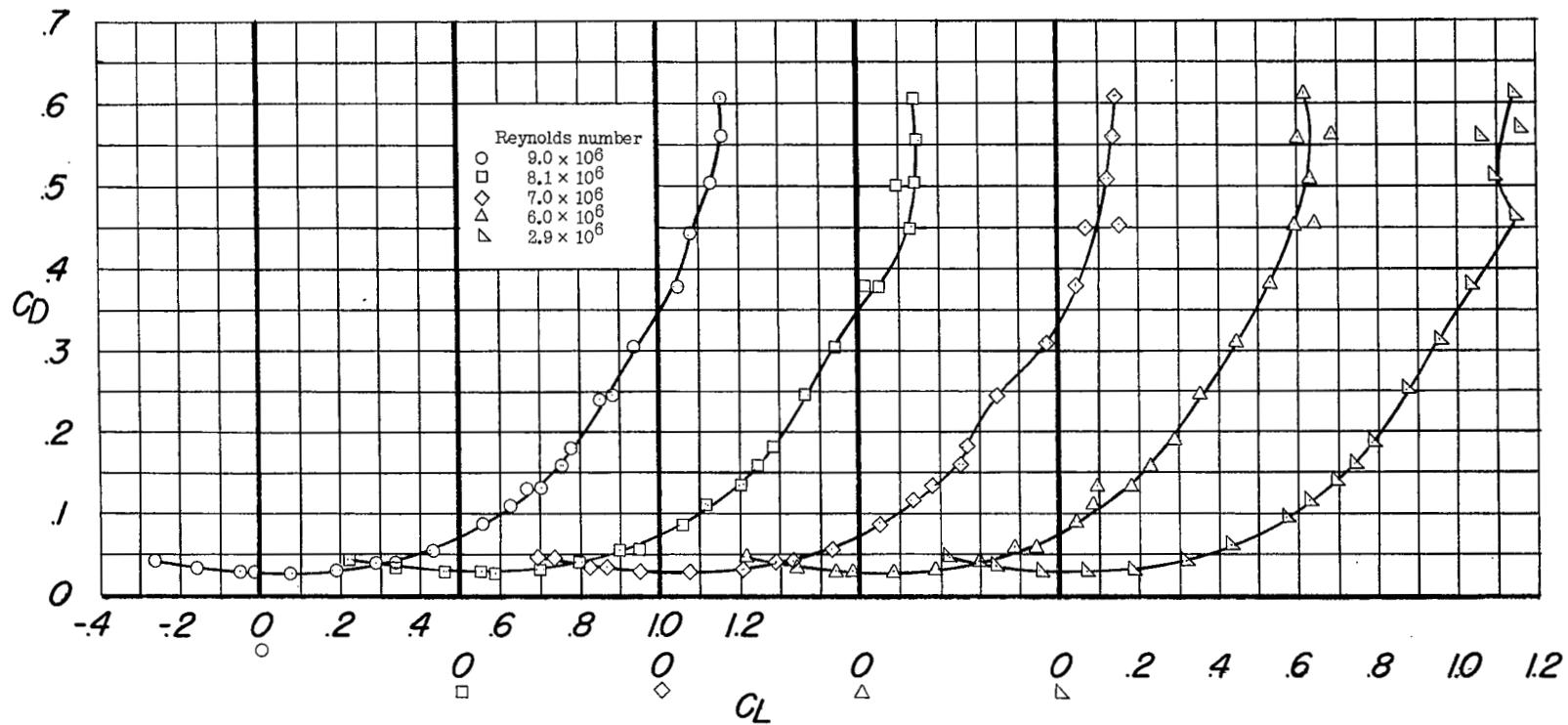
(d) C_D against C_L .

Figure 26.- Concluded.

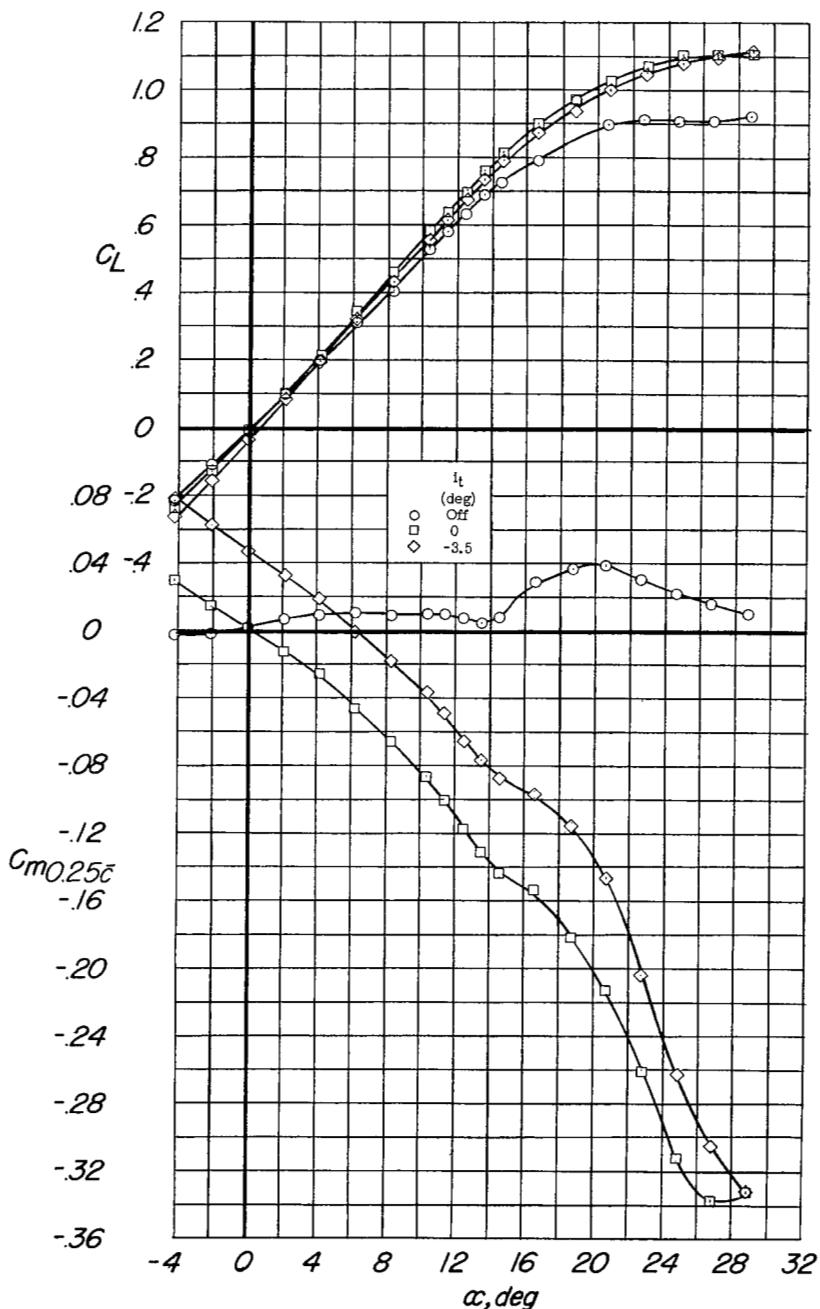
~~CONFIDENTIAL~~(a) C_L and $C_{m,0.25c}$ against α .

Figure 27.- Longitudinal characteristics of the model equipped with a transonic-type elliptical wing-root inlet and leading-edge flaps drooped 7.5° . Configuration: A + V + I_{TE} + (-0.123)T + N_{7.5}; center-of-gravity location, $0.25\bar{c}$.

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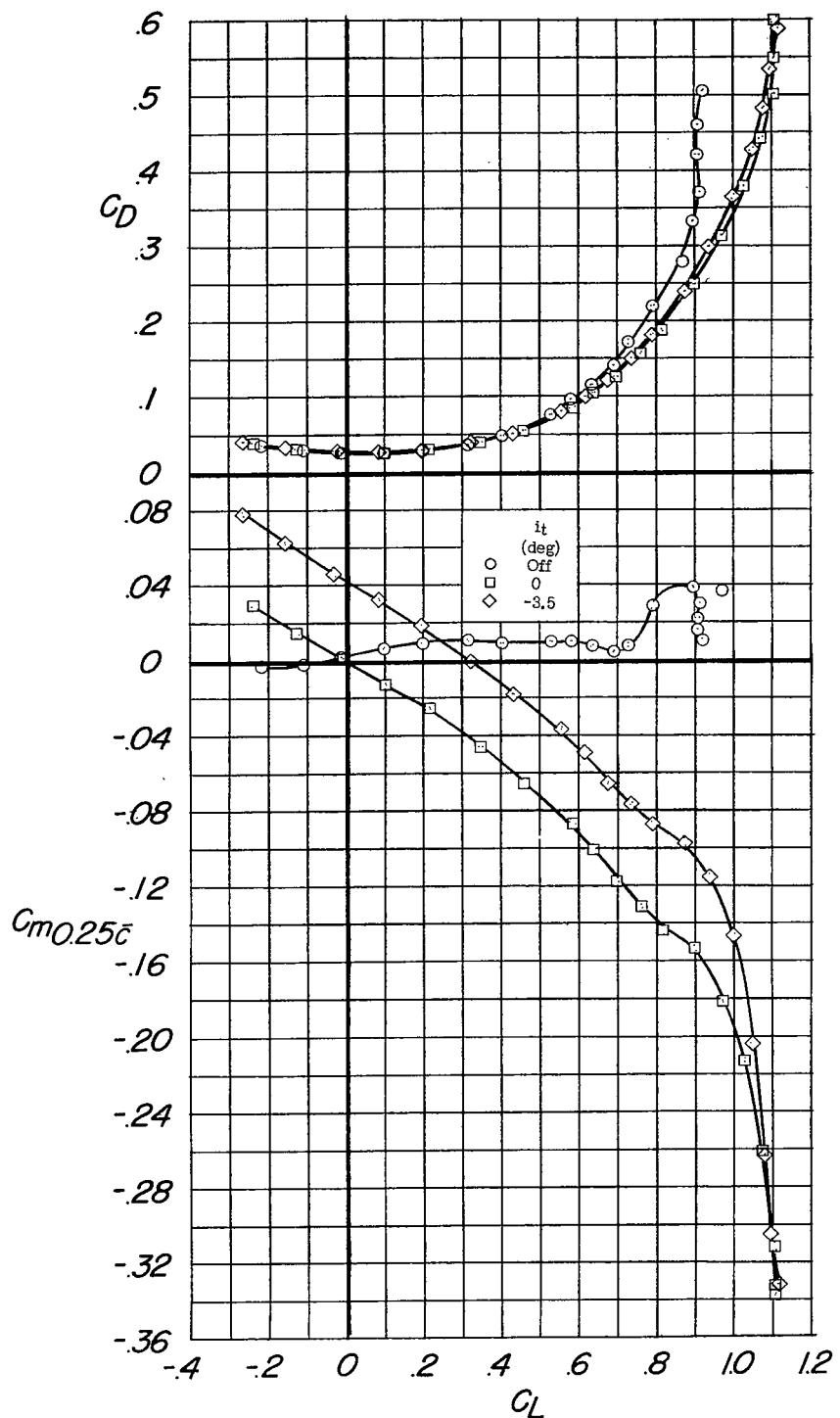
(b) C_D and $C_{m0.25\bar{c}}$ against C_L .

Figure 27.- Concluded.

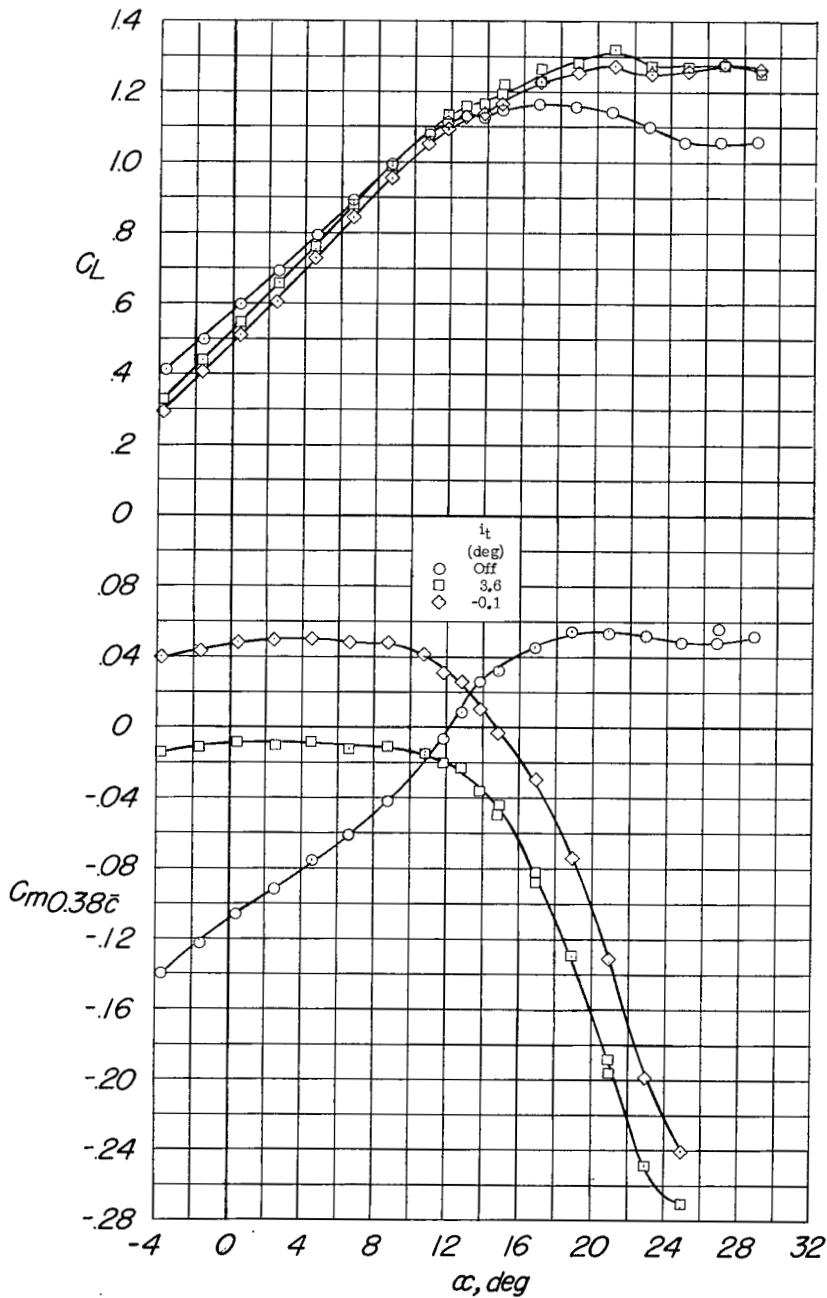
(a) C_L and $C_{m0.38c}$ against α .

Figure 28.- Longitudinal characteristics of the model equipped with a transonic-type elliptical wing-root inlet, 70-percent-span trailing-edge flaps deflected 46° , and the leading-edge flaps drooped 20° . Configuration: A + V + I_{TE} + (-0.123)T + 0.70F₄₆ + N₂₀ + E₀₄₅₀; center-of-gravity location, $0.38\bar{c}$.

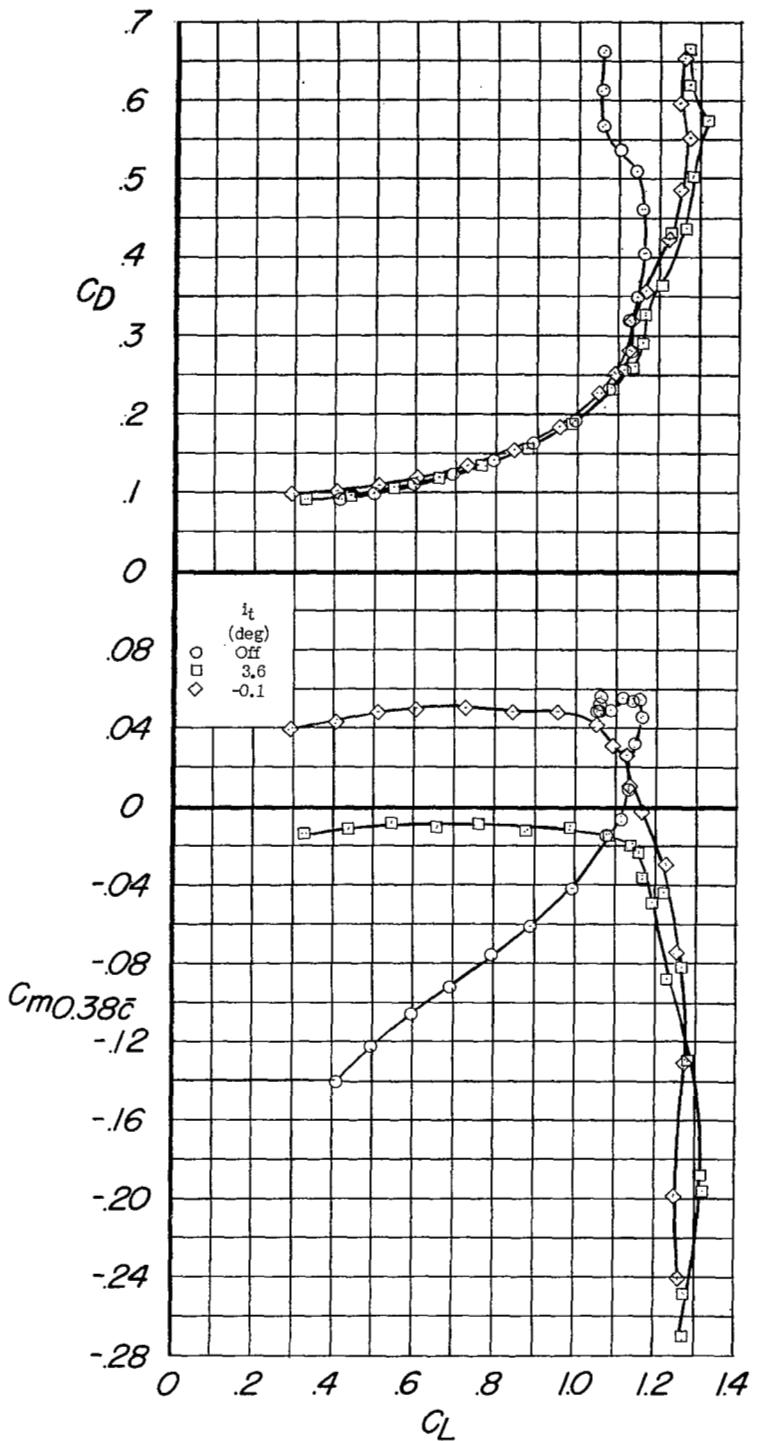
(b) C_D and $C_{m0.38c}$ against C_L .

Figure 28.- Concluded.

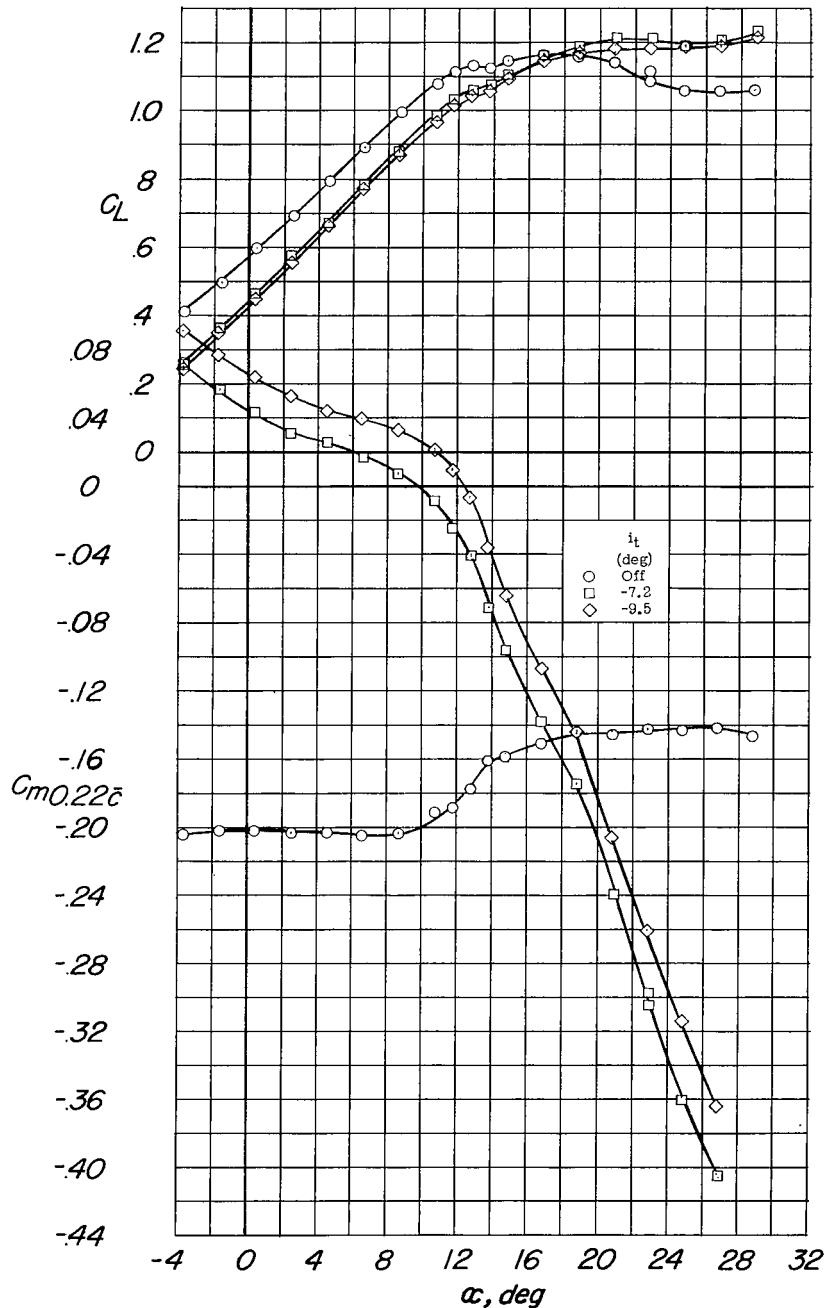
(a) C_L and $C_{m0.22\bar{c}}$ against α .

Figure 29.- Longitudinal characteristics of the model equipped with a transonic-type elliptical wing-root inlet, 70-percent-span trailing-edge flaps deflected 46° , and the leading-edge flaps drooped 20° . Configuration: A + V + I_{TE} + (-0.123)T + 0.70F₄₆ + N₂₀ + E₀⁴⁵⁰; center-of-gravity location, $0.22\bar{c}$.

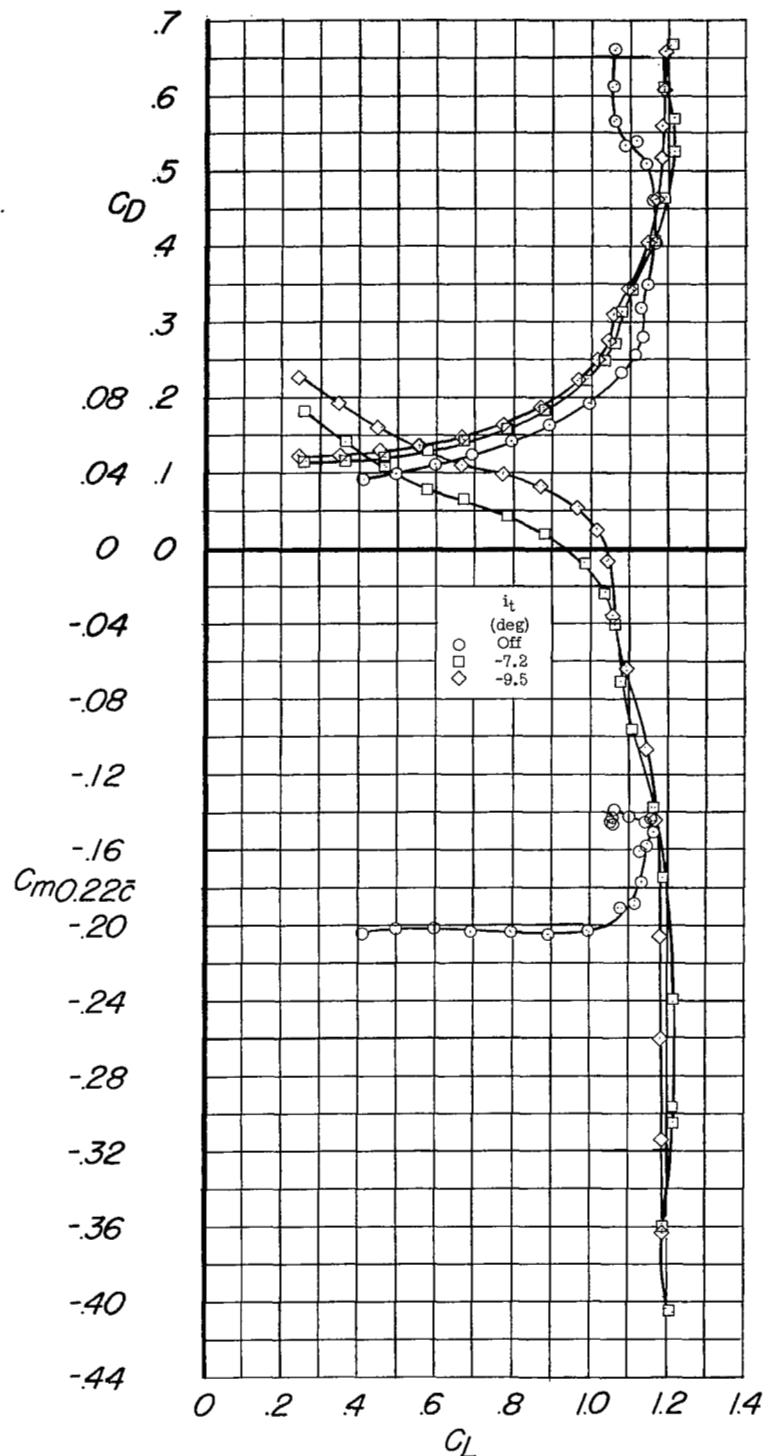
(b) C_D and $C_{m0.22\bar{c}}$ against C_L .

Figure 29.- Concluded.

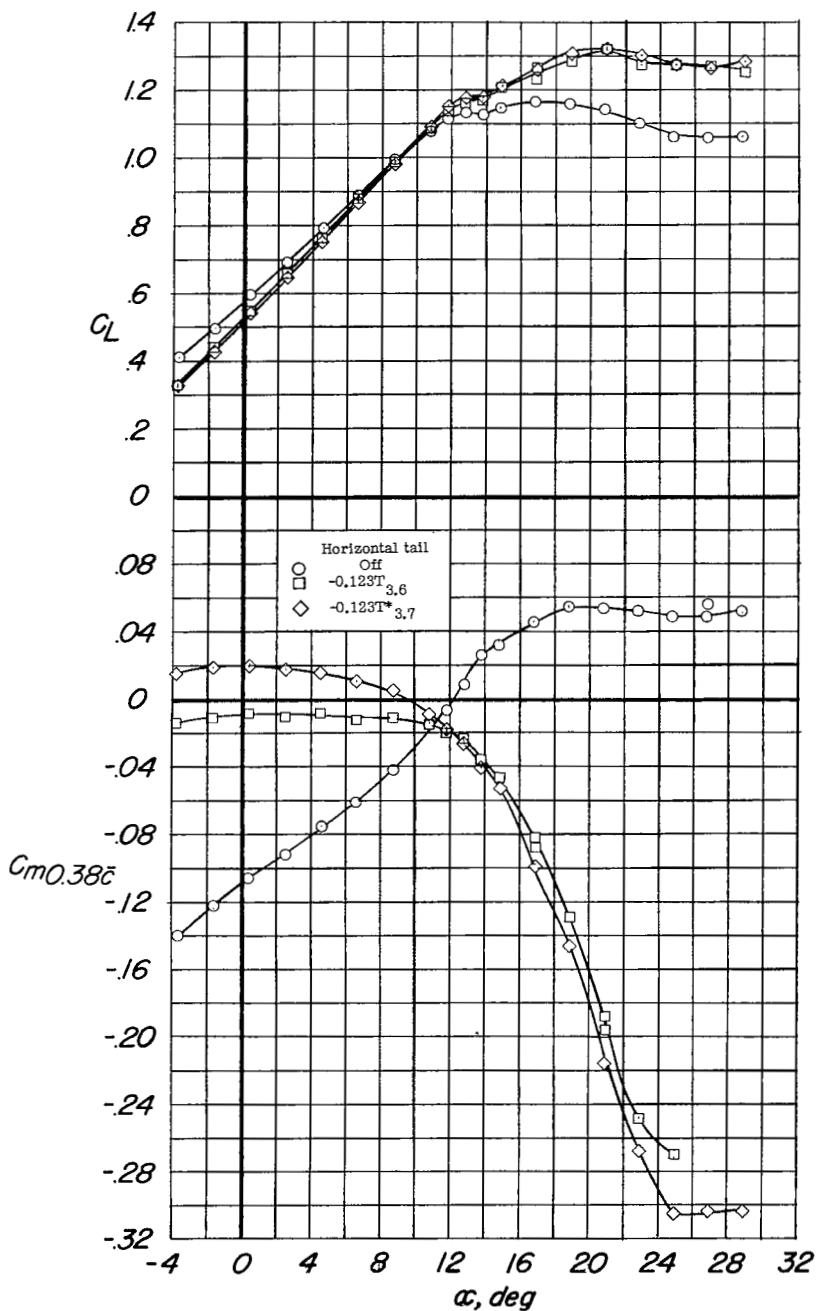
(a) C_L and $C_{m0.38c}$ against α .

Figure 30.- Longitudinal characteristics of the model equipped with a transonic-type elliptical wing-root inlet, an increased span horizontal tail, 70-percent-span trailing-edge flaps deflected 46° , and the leading-edge flaps drooped 20° . Configuration: A + V + I_{TE} + $(-0.123)T + 0.70F_{46} + N_{20} + E_0^{450}$; center-of-gravity location, $0.38\bar{c}$.

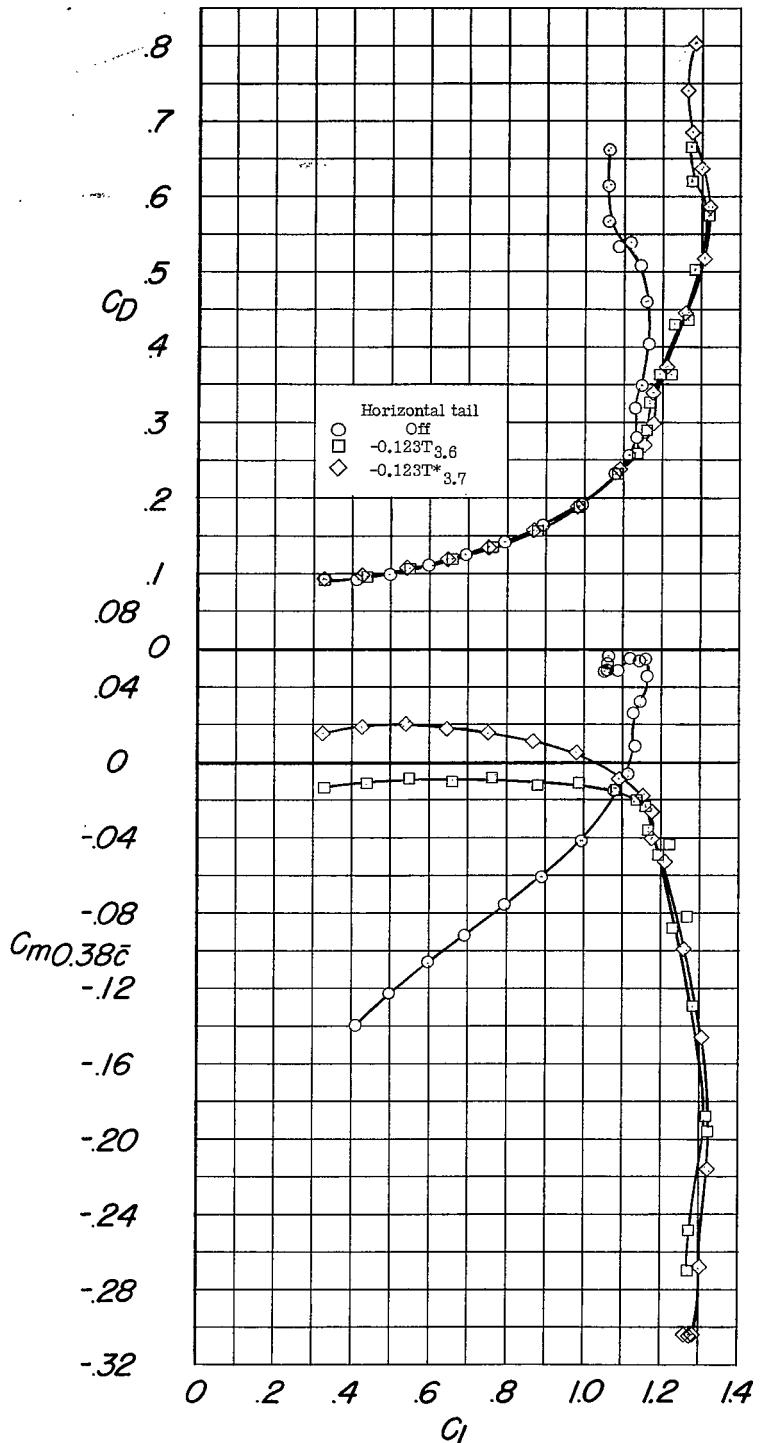
~~CONFIDENTIAL~~(b) C_D and $C_{m0.38c}$ against C_L .

Figure 30.- Concluded.
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